NYSERDA FlexTech Study

Rhinebeck Village Hall 76 East Market Street



Submitted to: NYSERDA Efficiency Planning & Engineering 17 Columbia Circle Albany, NY 12203-6399

Submitted from: M/E Engineering, P.C. 60 Lakefront Boulevard, Suite 320 Buffalo, NY 14202

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Village of Rhinebeck Rhinebeck Village Hall 76 East Market Street Rhinebeck, New York 12572

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EXECUTIVE SUMMARY

A comprehensive analysis of the Rhinebeck Village Hall, located at 76 East Market Street, in Rhinebeck NY, was conducted, with the primary goal of identifying and analyzing energy conservation measure upgrades that will have the largest impact on reducing the building's energy use. The services included performing an ASHRAE Level 1+ Audit and energy analysis to calculate and compare the annual energy consumption of various energy conservation measures and determine an estimated first cost, simple payback, estimated maintenance impact, and basic feasibility associated with each option.

M/E Engineering, P.C. performed a site inspection in September, 2021. For the purposes of this study, existing HVAC, lighting, electrical, domestic hot water and envelope systems were surveyed. The walk-through entailed observing existing systems and their operations, including obtaining equipment nameplate data, reviewing drawings, discussing concerns of the building owner, and verifying operational schedules. Energy Conservation Measures have been evaluated, and are summarized below.

EEM No.	Energy Efficiency Measure Description	Annual Electric Savings [kWh]	Electric Peak Demand Savings [kW]	Annual Electric Cost Savings [\$]	Annual Fossil Fuel Savings [Gal]	Annual Fossil Fuel Savings [mmBtu]	Annual Fossil Fuel Savings [\$]	Total Energy Consumption Savings [mmBtu]	Total Annual Cost Savings [\$]	Estimated EEM Cost [\$] (total)	Simple Payback [Years]
1	High-Efficiency Lighting	15,500	7.71	\$2,581	-185	-26	-275	26.95	\$2,306	\$29,500	12.8
2	Envelope Improvements- Roof and Wall	2,351	2.19	\$392	1,114	156	1,653	163.95	\$2,044	\$142,305	69.6
3a	Code RTU with DX cooling	-113,144	4.46	-\$18,843	4,329	606	6,424	219.84	-\$12,419	\$118,947	-9.6
3b	High Efficient RTU w/DX cooling	-93,463	8.82	-\$15,566	5,045	706	7,487	387.26	-\$8,079	\$160,158	-19.8
3c	High Efficient Heat Pump	3,226	10.12	\$537	5,045	706	7,487	717.26	\$8,024	\$212,902	26.5
3d	VRF System	5,067	12.53	\$844	5,045	706	7,487	723.54	\$8,330	\$240,506	28.9
3e	Geothermal System	6,144	10.09	\$1,023	5,045	706	7,487	727.22	\$8,510	\$487,178	57.2
4a	DHW Propane Fired Unit	7,676	0.17	\$1,278	-48	1	-234	26.90	\$1,044	\$10,740	10.3
4b	DHW Electric Unit	224	0.04	\$37	120	17	178	17.53	\$215	\$9,240	43.0
4c	DHW Air Source Heat Pump	5,019	0.06	\$836	120	17	178	33.89	\$1,014	\$16,224	16.0
4d	DHW Geothermal Well Field	5,603	0.07	\$933	120	17	178	35.89	\$1,111	\$19,224	17.3
5	Appliance Replacement & Hood Controls	6,026	1.02	\$1,004	163	23	241	43.32	\$1,245	\$15,427	12.4

Several of the energy efficiency measures evaluated for this project have shown that their implementation will reduce the energy and carbon use of the facility. Some of these measures would also provide an additional benefit of improving occupant comfort by eliminating drafts, improving the lighting, optimizing system controls, consolidating air conditioning equipment and providing a more uniform space temperature profile, as well as addressing ventilation and filtration for a healthier building environment.

The measures that are recommended include EEM 1 high-efficiency lighting, EEM 2 addressing air infiltration, EEM3 3d VRF selecting an HVAC system upgrade, EEM 4c selecting a domestic hot water system upgrade, and EEM 5 appliance replacement and hood heat/smoke control. Discussion of these recommendations can be found in the "Energy Analysis" section of the report. Implementation incentives may be available but are not guaranteed, subject to change, are contingent on available funding, program eligibility and acceptance.

NYSERDA PROJECT SUMMARY SHEET

BASELINE ENERGY SUMMARY

	Electric (kWh)	Natural Gas (therms)	#2 Oil (gallons)	#4 Oil (gallons)	#6 Oil (gallons)	Steam (lbs.)	Propane (gallons)	Coal (tons)	Other (MMBtu)	Total Baseline Use (MMBtu)
Baseline Energy Use	34,663.0		6,131.1				286.1			996.7
Average Utility Rate	\$0.17		\$1.48				\$2.45			Total Annual Cost (\$)
Baseline Annual Cost	\$5,773		\$9,099				\$700			\$15,572

ENERGY SAVINGS SUMMARY

			Elec	ctric		Energy		Cost		
Measure Description	Measure Status ¹	Fuel Savings Type ²	Supply Savings (kWh)	Demand Savings (kW)	Fuel Savings (MMBtu)	Savings to Total Baseline Use (%) ³	Annual Cost Savings	Savings to Total Annual Cost (%) ⁴	Project Cost	Simple Payback (Years)
EEM - 1 High Efficency Lighting	R	Oil2	15,500	7.71	-26.0	2.7%	\$2,306	14.8%	\$29,500	12.8
EEM - 2 Evelope Improvments- Roof, Wall	R	Oil2	2,351	2.19	155.9	16.4%	\$2,044	13.1%	\$142,305	69.6
EEM - 3a Code RTU with DX cooling	NR	Oil2	-113,144	4.46	606.0	22.1%	-\$12,419	-79.8%	\$118,947	-9.6
EEM - 3b High Efficient RTU w/DX Cooling	NR	Oil2	-93,463	8.82	706.2	38.9%	-\$8,079	-51.9%	\$160,158	-19.8
EEM - 3c High Efficient Heat Pump	NR	Oil2	3,226	10.12	706.2	72.0%	\$8,024	51.5%	\$212,902	26.5
EEM - 3d VRF System	R	Oil2	5,067	12.53	706.2	72.6%	\$8,330	53.5%	\$240,506	28.9
EEM - 3e Geothermal System	NR	Oil2	6,144	10.09	706.2	73.0%	\$8,510	54.6%	\$487,178	57.2
EEM - 4a DHW Propane Fired Unit	NR	Oil2	7,676	0.17	0.7	2.7%	\$1,044	6.7%	\$10,740	10.3
EEM - 4b DHW Electric Unit	NR	Oil2	224	0.04	16.8	1.8%	\$215	1.4%	\$9,240	43.0
EEM - 4c DHW Air Source Heat Pump	R	Oil2	5,019	0.06	16.8	3.4%	\$1,014	6.5%	\$16,224	16.0
EEM - 4d DHW Geothermal Well Field	RNE	Oil2	5,603	0.07	16.8	3.6%	\$1,111	7.1%	\$19,224	17.3
EEM - 5 Appliance Repl & Hood Ctrl	R	Oil2	6,026	1.02	22.8	4.3%	\$1,245	8.0%	\$15,427	12.4
		TOTAL (AII):	-149,771	57.29	3,635	313.4%	\$13,345	85.7%	\$1,462,352	109.6
TOTAL (I	Recommer	nded Only):	39,566	23.58	892	103.1%	\$16,050	103.1%	\$463,186	28.9

Me	asure Status ¹	Fuel Sa	aved	MMBtu Con	version Factors	Notes:
1	Implemented	Elec	Electric	Btu	1,000,000	² Fuel Savings Type: Indicate the reported MMBtu savings fuel type. Select the predominant fuel type if there are MMBtu
R	Recommended	NGas	Natural Gas	kWh	0.003412	savings from multiple fuel sources ³ Energy Savings to Total Fuel Baseline Use is a comparison of the total electric & fuel savings to the total baseline energy use
RS	Further Study Recommended	Oil2	#2 Oil	therms	0.1	Energy savings to Total Puel Baseline use is a comparison of the total electric & rule savings to the total baseline energy use ⁴ Cost Savings to Total Annual Cost is a comparison of the total annual cost savings to the total baseline annual energy cost
NR	Not Recommended	Oil4	#4 Oil	#2 gallon	0.139	Cost Savings to Total Alindar Cost is a comparison of the total annual cost savings to the total baseline annual energy cost
RN	E Recommeded Mutually Exclusive	Oil6	#6 Oil	#4 gallon	0.1467	Instructions:
ME	Mutually Exclusive to Recommended Option	Steam	District Steam	#6 gallon	0.15	* Fill in the light blue cells, as appropriate. White cells will auto-calculate.
RN	E Recommended Non-Energy	LPG	Propane	Steam lbs.	0.0012	* Energy savings must be presented as savings at the customer's utility meter(s), not at the individual building or tenant space
		Coal	Coal	LPG gallon	0.0915	* Update the baseline energy use conversion factors in the 'References' tab, as necessary
		Other	Other	Coal tons	24	* Unhide rows to enter more measures, as necessary

PROJECT OVERVIEW

The overall goal of this project is to provide a comprehensive analysis of the Rhinebeck Village Hall to identify options for energy improvements including upgrading / replacing the building HVAC systems, and to quantify the energy and cost impact of implementing the measures. This study is intended to focus on eligible areas of study under the NYSERDA FlexTech Program, which consists of the investigation of opportunities to reduce energy. An additional goal is to achieve carbon savings via load reduction and load shifting, and conversion to carbon free fuel. This study includes energy conservation measure analysis and strategic carbon footprint reduction planning, the integration of renewable generation, and the feasibility of incorporating clean heating and cooling technologies where possible. An additional objective is for the Owner to make use of the study as a roadmap to aid in identifying and planning for potential future capital projects, including potential clean energy projects. This includes calculating the annual energy savings associated with various energy efficiency measures, determining an estimated first cost, simple payback, estimated maintenance impact, and basic feasibility associated with each measure.

CONTACT SHEET

Building

Rhinebeck Village Hall 76 East Market Street Rhinebeck, New York 12572

NYSERDA Representative

Vibhor Dutt - Project Manager Efficiency Planning & Engineering NYSERDA 17 Columbia Circle Albany, NY 12203-6399 P: 518-862-1090 x3656 Vibhor.Dutt@nyserda.ny.gov

<u>Owner</u>

Vanessa Bertozzi Village Trustee 76 East Market Street Rhinebeck, New York 12572 845-876-7015 TrusteeBertozzi@villageofrhinebeckny.gov

Primary Energy Consultant

Melanie Stachowiak PE - Partner M/E Engineering, P.C. 60 Lakefront Blvd, Suite 320 Buffalo, NY 14202 (716) 845-5092 x1207 mgstachowiak@meengineering.com

Krista Wayne - Energy Engineer M/E Engineering, P.C. 60 Lakefront Blvd, Suite 320 Buffalo, NY 14202 (716) 845-5092 kewayne@meengineering.com

Engineering Consultant

Ryan Meadows - Senior Engineer M/E Engineering, P.C. 433 State Street, Suite 410 Schenectady, NY 12305 (518) 533-2171 rdmeadows@meengineering.com

EXISTING CONDITIONS

The Village of Rhinebeck, located in Central Hudson territory, Duchess County NY, is committed to mitigate climate change. The Village is participating in NY State's Climate Smart Communities Program and have set up a Climate Smart Task Force, which is "working to encourage, implement, and quantify the village's efforts to address the climate crisis". The goal is to make the village a more "just, resilient, and livable future in Rhinebeck".

The Rhinebeck Village Hall, is a 12,000 square foot, two-story facility built in 1970, comprised of a Village Hall and Fire Station in the same building that serves the community. In addition to the firetruck storage and maintenance bays, the facility houses Mayoral offices, clerk, radio/dispatch, offices of zoning and planning, meeting/court, kitchen, lounge/recreation and support spaces such as storage, restroom, lobby, corridor, stairs, and mechanical/electrical. The building contains a partial basement, a first, and a second floor. The building is of masonry construction with a brick façade with CMU backup and painted gypsum interior finish with no insulation, and flat EPDM roofs above a ventilated interstitial attic space. The roof was replaced in 2001 with a 20 year warranty by Carlisle (expired May 16, 2021). The building's windows replaced in 2011, are generally double panes with argon and low-e double hung, operable sash type. The fire hall contains four overhead garage doors. The typical operating hours are 10am-4pm, Monday-Friday.

The lighting in the facility is mostly fluorescent tube T-8 fixtures with prism lenses, with some lighting replaced with LED (i.e. track lighting in Radio/Dispatch room). Other spaces have track lighting with MR-16 halogen bulbs. Primary electrical service is 200A, 208V/3Ph and enters at the basement mechanical room. A generator is onsite for back-up power in case of an outage. Roof mounted solar PV panels produce power to supplement the building's purchased electricity.

The existing HVAC heating system consists of an oil fired hot water boiler with a 2-pipe pipe distribution system. The Weil McLain Series 84 cast iron boiler, original to the building, is fired by a Beckett model 301 CRD burner indicating 3 - 7.0 Gallons per hour of fuel consumption (depending on the combustion head adjustment). Number 2 heating oil has an energy content between 135 to 140 kBTU/gallon which translates to a burner input of 400 - 1,000 MBH. With a combustion efficiency of 80% the boiler's peak output would be approximately 800 MBH.

The boiler receives its oil from two 330 gallon (319 usable) residential fuel tanks also in the basement adjacent to the boiler in the former location of the generator (now at grade). The tanks were installed new in 2018. The flue is routed up through the building in a masonry chimney. Combustion air is provided to the room via a wall mounted intake louver at the areaway. There are reportedly three (3) thermostats within the building which will enable the boiler to fire. The heating is routed to fin-tube radiation and convectors around the building's perimeter via a circulator pump. The fire house garage has four (4) horizontal unit heaters controlled by a single thermostat.

No central cooling nor ventilation systems are present within the building. Some rooms have openings under the windows (original to the building) for through-wall air conditioners. Other office spaces and the Lounge have window air conditioners installed in the operable windows. In one case a portable 'Move-n-cool' style portable AC unit rejects heat via a duct through a window panel. Natural ventilation is only accessible via operable windows. Ventilation and comfort control is of concern in the facility especially in areas that have been reworked and walls constructed. No whole building BMS is present, only equipment manufacturer controls (either built-in or remote).

The restrooms are equipped with ceiling exhaust fans that are ducted to the exterior of the building. They are enabled by wall mounted switches. The kitchen has a hood over the ranges and exhaust fan on roof. The fire house has vehicle exhaust capture systems.

Heating hot water for the kitchen and restrooms is provided by single-block model 32E oil-fired 32- gallon tank type water heaters located adjacent to the heating boilers. The Village desires to eliminate the fuel oil.

A generator is on site, providing emergency power. This is fired by propane. Propane also serves the kitchen ranges and cooktops. There is no natural gas on site.

UTILITY ANALYSIS

Utility Rates

Utilities to the building are being delivered via Central Hudson Gas and Electric Corporation for electric. The building is also provided with #2 Fuel Oil and Propane. The utility rate utilized for the calculations are indicated in the summary table below which is based on utility bills. Due to low occupancy and gaps in data during the COVID pandemic, the 2018-2019 utility bills were utilized for electric, and the 2019-2020 utility bills for fuel oil and propane were utilized, generating the average combined rates below. As you can see the fuel oil usage in February and March of 2020.

	Rhinebeck Village Hall - Electrical										
	<u>2018-2019</u>			2019-2020		2020-2021					
Month	Electric Usage (kWh)	Electric Cost (\$)	Month	Electric Usage (kWh)	Electric Cost (\$)	Month	Electric Usage (kWh)	Electric Cost (\$)			
Jun-18	1,743	\$414.22	Jun-19	428	\$278.63	Jun-20	COVID19	COVID19			
Jul-18	3,772	\$576.26	Jul-19	2,260	\$414.72	Jul-20	COVID19	COVID19			
Aug-18	3,980	\$623.17	Aug-19	3,267	\$607.55	Aug-20	COVID19	COVID19			
Sep-18	3,314	\$596.26	Sep-19	1,838	\$406.94	Sep-20	11479	\$3,440.66			
Oct-18	2,343	\$438.41	Oct-19	1,461	\$376.14	Oct-20	1188	\$409.37			
Nov-18	3,292	\$547.06	Nov-19	2,460	\$406.80	Nov-20	2488	\$464.23			
Dec-18	4,385	\$486.07	Dec-19	4,103	\$542.99	Dec-20	3841	\$540.15			
Jan-19	4,697	\$514.32	Jan-20	2,965	\$525.02	Jan-21	0	\$0.00			
Feb-19	3,404	\$510.19	Feb-20	3,775	\$541.38	Feb-21	9029	\$1,351.83			
Mar-19	1,631	\$461.78	Mar-20	0	COVID19	Mar-21	1967	\$555.20			
Apr-19	876	\$305.16	Apr-20	0	COVID19	Apr-21		\$405.54			
May-19	1,226	\$299.92	May-20	0	COVID19	May-21		\$271.34			
TOTAL	34,663	\$5,772.82	TOTAL	22,557	\$4,100.17	TOTAL	29,992	\$7,438.32			

Rhinebeck Village Hall - Fuel Oil									
	2019-2020		<u>2020-2021</u>						
Month	Fuel Oil	Fuel Oil	Month	Fuel Oil	Fuel Oil				
MONUT	(gallons)	Cost (\$)	WORT	(gallons)	Cost (\$)				
Jun-19	0	\$0.00	Jun-20	0	\$0.00				
Jul-19	0	\$0.00	Jul-20	0	\$0.00				
Aug-19	0	\$0.00	Aug-20	0	\$0.00				
Sep-19	0	\$0.00	Sep-20	0	\$0.00				
Oct-19	494	\$1,068.68	Oct-20	105	\$138.10				
Nov-19	90	\$196.82	Nov-20	441	\$622.75				
Dec-19	503	\$1,094.54	Dec-20	922	\$1,555.79				
Jan-20	999	\$2,245.89	Jan-21	544	\$1,004.27				
Feb-20*	772	\$1,598.43	Feb-21	1,426	\$2,855.03				
Mar-20*	482	\$920.23	Mar-21	1,882	\$1,440.69				
Apr-20	505	\$849.35	Apr-21	503	\$1,034.44				
May-20	187	\$310.07	May-21	310	\$447.87				
TOTAL	4,032	\$8,284.01	TOTAL	6,131	\$9,098.94				

*COVID greatly impacted the fuel consumption during these months

Rhinebeck Village Hall - Propane									
	2019-2020		<u>2020-2021</u>						
Month	Propane	Propane	Month	Propane	Propane				
WORT	(gallons)	Cost (\$)	MONUN	(gallons)	Cost (\$)				
Jun-19	0	\$0.00	Jun-20	0	\$0.00				
Jul-19	0	\$0.00	Jul-20	0	\$0.00				
Aug-19	0	\$0.00	Aug-20	0	\$0.00				
Sep-19	0	\$0.00	Sep-20	0	\$0.00				
Oct-19	163.3	\$332.23	Oct-20	0	\$0.00				
Nov-19	119.6	\$266.71	Nov-20	81.3	\$179.06				
Dec-19	0	\$0.00	Dec-20	0	\$0.00				
Jan-20	0	\$0.00	Jan-21	0	\$0.00				
Feb-20	0	\$0.00	Feb-21	0	\$0.00				
Mar-20	0	\$0.00	Mar-21	204.8	\$521.22				
Apr-20	0	\$0.00	Apr-21	0	\$0.00				
May-20	0	\$0.00	May-21	0	\$0.00				
TOTAL	283	\$598.94	TOTAL	286	\$700.28				

Rhinebeck Village Hall - Utility Cost								
Electricity	\$0.17	\$/kWh						
Fuel Oil	\$1.48	\$/gallon						
Propane	\$2.45	\$/gallon						

Benchmarking

The calculated existing Energy Utilization Index (EUI) for the existing 12,000 square foot building is 91.0 kBtu/sf. The national median EUI, according to Energy Star Portfolio Manager, for a similar type buildings is 52.9 kBtu/sf for Office and 63.5 kBtu/sf for Fire Station.

	Benchmarkin	ng	
Area Description	Area (SF)	Energy Consumption (mmBtu)	EUI (kBtu/sf)
Typical Office	8,400	444	52.9
Typical Fire Station	3,600	229	63.5
Total	12,000	673	56.1
Rhinebeck Village Hall	12,000	994	93.5

APPROACH / METHODOLOGY

The analysis to estimate annual energy consumption and cost was performed using NYS Technical Resource Manual (TRM) v 8.0 spreadsheet analysis unless otherwise noted below. Typically NYS Technical Resource Manual (TRM) 8.0 calculations often are more than adequate to address HVAC system comparisons so this is the traditional first choice. BIN data spreadsheet analysis typically are used where TRM is not appropriate i.e. additional detail and exceptional calculations. A simplified eQuest whole building zoned block modeling may be used where there are interactive measures or complex systems (i.e. hybrid system type not addressed by the TRM). Assumptions are made for components not yet designed. The intent is to capture the incremental savings of the measures identified for study.

The following energy conservation measures were evaluated:

- <u>EEM-1 High Efficiency Lighting</u> This measure includes the evaluation of replacing fixtures with LED lighting, and the addition of occupancy sensors.
- <u>EEM-2 Envelope Improvements</u> This measure included the addition of wall insulation, and roof replacement. This measure required an inventory of existing wall construction and insulation thicknesses, roof types and insulation thicknesses, and the associated square footages associated with each of these envelope components.
- <u>EEM-3 HVAC system replacement</u> Possible upgrades to improve efficiency. The existing HVAC system is an oil fired how water boiler with a 2-pipe pipe heating system with perimeter fintube, hydronic unit heaters, and through-wall and portable A/C units, with ventilation limited to natural ventilation and some exhaust. The desire is to incorporate air conditioning and ventilation, so a one for one replacement is not being considered. Five (5) options were evaluated for HVAC system replacement:
 - Traditional code compliant packaged constant volume rooftop unit with DX cooling and electric resistance heating.
 - High efficiency packaged variable volume rooftop unit with DX cooling and electric resistance heating. Electric reheat.
 - Packaged variable air volume roof-mounted heat pump high efficiency unit with reversible modes and energy recovery, ducted to provide both conditioning and ventilation air, and electric reheat.
 Split systems to handle remaining load if there are spaces that cannot be addressed by the roof unit or have loads that significantly deviate from the rest of the building.
 - Variable Refrigerant Flow (VRF) System Distributed indoor units with heat recovery capability, and a dedicated outdoor air unit (heat pump with reversible flow) with energy recovery.
 - Geothermal System geothermal heat pump system, including well field, heat pumps, ventilation and control upgrades.
- <u>EEM-4 Domestic Hot Water Heating</u> Replacement of existing electric domestic water heaters with a DHW system that aligns with the HVAC upgrades. Four (4) were evaluated for DHW system replacement:
 - Propane Fired Heater
 - Electric Resistance Heater
 - High Efficiency Air Source Heat Pump
 - Hot water heater served by geothermal well field
- <u>EEM-5 Appliance Replacement and Hood Controls</u>
 - Reduction in plug loads due to kitchen appliance replacement.
 - VFD smoke/heat sensing for kitchen hoods

For each measure analyzed, the following has been provided:

- Measure Description. Brief description of each system, system comparison, and feasibility overview (i.e. pros / cons, project impact, etc.).
- Detailed annual energy and cost analysis complete with anticipated savings.
- High level budgetary order of magnitude opinion of probable construction cost using a combination of RS Means, project experience, and other industry standard methods. This includes a breakdown for equipment, material, and labor.
- Simplified annual maintenance costs estimated using RS Means Facilities Maintenance and Repair Costs as a guide. These will include the identification of differences between the HVAC systems only and will not identify all maintenance associated with the building.
- Simple payback of each measure.
- Measure reporting in tabular format utilizing NYSERDA's project summary template.

ENERGY ANALYSIS

EEM-1: HIGH-EFFICIENCY LIGHTING

This measure is intended to include the evaluation of replacing fixtures with LED lighting, and the addition of occupancy sensors. A survey of the existing light fixtures and controls was performed, with space usage types, square footage, and hours of operation noted.

Most of the lighting in the existing buildings is provided by standard T8 tube florescent fixtures with prism lenses. Some room's track lighting have had the bulbs replaced with LED such as in the Radio/Dispatch. Other spaces' tracking lighting is still MR-16 halogen bulbs. Replacing all existing lighting with LED lighting technology provides energy savings by reducing the required input energy to obtain the same lighting levels. Due to the low (inadequate) lighting levels in the building and some replacements already taking place, a combination of the inventory and assumed code compliant levels were used to determine the baseline watts per square foot for the calculations.

Baseline (Existing) Assumptions:

- Office: 1.1 W/SF lighting power density (LPD).
- Firetruck Parking: 0.9 W/SF lighting power density (LPD).
- Exterior: 6 building mounted fixtures, 150W each
- Proposed Assumptions:
 - Office: This was assumed to be a 30% LPD improvement over code as is typical of high efficient buildings. This resulted in an LPD of 0.55 W/sf and a 10% credit was taken for Occupancy Sensors resulting in a 0.50 W/sf LPD
 - Firetruck Parking: This was assumed to be a 30% LPD improvement over code as is typical of high efficient buildings. This resulted in an LPD of 0.37 W/sf and a 10% credit was taken for Occupancy Sensors resulting in a 0.33 W/sf LPD.
 - Exterior: 6 building mounted fixtures, 54W each

Γ			A	Electric	Annual	Annual	Annual	Annual	Total	Total		
			Annual	Peak	Electric	#2 Fuel	#2 Fuel	#2 Fuel	Energy	Annual	Estimated	Simple
	EEM	5, 11, 11, 11, 11, 11, 11, 11, 11, 11, 1	Electric	Demand	Cost	Oil	Oil	Oil Cost	Consumption	Cost	EEM Cost	Payback
	No.	Measure Description	Savings	Savings	Savings	Savings	Savings	Savings	Savings	Savings	[\$] (total)	[Years]
			[kWh]	[kW]	[\$]	[gallons]	[mmBtu]	[\$]	[mmBtu]	[\$]		
	1	High-Efficiency Lighting	15,500	7.71	\$2,581.46	-185	-25.96	-\$275.16	26.95	\$2,306.30	\$29,500.00	12.8

Table 4: EEM-1 Summary

The payback associated with providing high efficient LED lighting is approximately 13 years. This measure is recommended to be implemented.

EEM-2: ENVELOPE IMPROVEMENTS

This measure is intended to include the addition of wall insulation and a roof replacement with the addition of insulation. This also is intended to address the loss of heat via air infiltration at the second floor which cause the ceiling tiles to move due to the significant draft. Existing wall construction and insulation thickness, roof types and insulation thickness were noted, and the associated square footages associated with each of these envelope components was calculated. It is assumed that the roof insulation is roughly 2001 code compliant, and likely that the wall contains little to no insulation. This measure addresses the replacement of the existing roof with 6" of insulation and the furring out of the interior walls.

EEM-2 Envelope Improvements - Roof and Wall

Baseline (Existing) Assumptions:

- Built-up roof, 2001 installed, R=13
- Wall construction of face brick, air gap, CMU backup, painted gypsum board R=7
- Roof square footage calculated from plans, 5,400 sf
- Walls surface area calculated from plans, 6,888 sf
- Air Infiltration at ceiling of second floor
- Proposed Assumptions:
 - Roof: 4 inches of rigid insulation, R=5/inch, R=30 total
 - Walls same as baseline with an additional 3.5" stud cavity with 4" of compressed batt insulation at R-5/inch, R-23 total.
 - Air Infiltration minimized, air barrier installed.

Values modeled the same in both:

- Wall square footage minus windows calculated from plans
- Roof square footage calculated from plans
- Existing Cooling Efficiency 11.2 EER (maximum, 9.0 EER average), 11.6 IPLV maximum, small through-window and self-contained/portable AC Units
- Existing Heating Efficiency Existing Steam Boiler 80% efficiency.

		امريم	Electric	Annual	Annual	Annual	Annual	Total	Total		
	Energy Efficiency	Annual	Peak	Electric	#2 Fuel	#2 Fuel	#2 Fuel	Energy	Annual	Estimated	Simple
EEM	- 37 7	Electric	Demand	Cost	Oil	Oil	Oil Cost	Consumption	Cost	EEM Cost	Payback
No.	Measure Description	Savings	Savings	Savings	Savings	Savings	Savings	Savings	Savings	[\$] (total)	[Years]
		[kWh]	[kW]	[\$]	[gallons]	[mmBtu]	[\$]	[mmBtu]	[\$]		
2	Envelope Improvements -	0.054	2.40	¢204 50	4 4 4 4	455.00	¢4.050.00	402.05	¢0.044.47	¢440.004.50	<u> </u>
2	Roof and Walls	2,351	2.19	\$391.59	1,114	155.92	\$1,652.88	163.95	\$2,044.47	\$142,304.53	69.6

Table 5: EEM-2 Summary

The existing roof has solar panels mounted on it so the roof replacement will be somewhat more complex than a simple roof removal/replacement as the supports of the roofers will need to work around the solar panels. It may be more advantageous to apply the additional insulation inside the building IF a thermoshydro analysis shows that the dewpoint is located in an acceptable layer. Furring out of the interior walls may be costly due to the need to relocate wall mounted items. **EEM-2 is listed as recommended**, **however, we only partially recommend this measure**. When combining all EEM-2 items together, the payback is longer than the life of the systems, however addressing the air infiltration as a standalone measure is lucrative. We encourage addressing the air infiltration - making the improvement to the infiltration to reduce the draft will not only have an energy impact, but will also have a positive impact on occupant comfort. When you look at these measures separately, the approximate annual energy savings is as follows: Roof = \$380/yr; Walls = \$1,520/yr; Infiltration = \$2,050/yr.

EEM-3: HVAC SYSTEM REPLACEMENT

The existing system is an oil fired hot water boiler with a 2-pipe pipe heating system utilizing fintube and unit heaters, with through-wall and portable A/C units scattered throughout. The desire is to eliminate fuel oil and to incorporate air conditioning and ventilation, so a one for one replacement is not being considered. We have evaluated five (5) options for HVAC system replacement for possible upgrades to improve efficiency:

EEM-3a Traditional baseline code compliant constant volume rooftop unit with DX cooling and electric heating.

EEM-3b High efficient variable volume rooftop unit with DX cooling and electric heat with energy recovery and electric reheat.

EEM-3c High efficient variable volume packaged roof-mounted heat pump unit with reversible modes and energy recovery, ducted to provide both conditioning and ventilation air.

EEM-3d Variable Refrigerant Flow (VRF) System - distributed indoor units with heat recovery capability, and a dedicated outdoor air unit (heat pump with reversible flow) with energy recovery. EEM-3e Geothermal System - geothermal heat pump system, including well field, heat pumps, ventilation and control upgrades.

For all scenarios, the intent would be to separate out the Fire Truck Bay area so it could operate as relatively independent as a stand-alone zone, with its own controls, and likely dedicated AHU.

EEM-3a: Code RTU with DX Cooling

A traditional code compliant constant volume rooftop unit utilizing electric heating and DX cooling, has been evaluated as a proposed replacement system. One roof-mounted air handling unit was modeled, however in practice this would likely be divided up into a minimum of two, possibly three units to handle the varying exposures and uses i.e. Fire truck Bay, Second Floor, First Floor or meeting room. This would allow for better control especially since there are two floors and an assembly area with denser occupancy. A constant volume unit(s) would be a relatively simple system with the temperature and air flow delivered to each space designed according to the worst-case zone. Outdoor air would be delivered to the spaces as mixed air, so the unit(s) would be required to run continuously during all occupied hours to provide proper ventilation air. Energy recovery is not required for the system, and has not been included, however this is an option that could be included in the design and would make the system better than code.

Baseline (Existing) Assumptions:

- Oil fired hot water boiler, 800 mbh heating, 80% efficiency (oversized with system inefficiencies beyond boiler)
- Existing cooling via small through-window and portable A/C units, Cooling Efficiency 11.2 EER (maximum, 9.0 EER average), 11.6 IPLV

Proposed Assumptions:

- Rooftop unit, DX cooling, electric heating, constant volume
 - 12,000 CFM, 2,750 CFM OA
 - 300 mbh heating, 23 tons cooling
 - Code: 11.0 EER, 12.4 IEER cooling, 100% efficient heating (COP 1.0).

		امسمد	Electric	Annual	Annual	Annual	Annual	Total	Total		
ЕЕМ	Energy Efficiency	Annual	Peak	Electric	#2 Fuel	#2 Fuel	#2 Fuel	Energy	Annual	Estimated	Simple
	Energy Efficiency Measure Description	Electric	Demand	Cost	Oil	Oil	Oil Cost	Consumption	Cost	EEM Cost	Payback
No.	Measure Description	Savings	Savings	Savings	Savings	Savings	Savings	Savings	Savings	[\$] (total)	[Years]
		[kWh]	[kW]	[\$]	[gallons]	[mmBtu]	[\$]	[mmBtu]	[\$]		
3a	Code RTU with DX cooling	-113,144	4.46	-\$18,843.10	4,329	606.00	\$6,423.90	219.84	-\$12,419.20	\$118,946.80	-9.6

Table 6: EEM-3a Summary

This measure shows a significant increase in electric consumption. This is because the existing facility is not fully air conditioned, not fully ventilated, and this minimally compliant system type includes electric resistance heating. This measure would require ductwork to extend throughout the space, Likely run above ceilings or exposed and ceiling hung. In some areas the ducts could be run in the corners of the rooms and displacement ventilation diffusers could be installed to create a healthier environment (supply low, return high, remove contaminants). Chases may be necessary to run between floors for the ductwork. The existing fintube could be removed or a supplemental electric boiler may be installed to provide greater comfort at the perimeter. Perimeter fintube was not modeled and the demolition/wall repair costs were not included in the budgetary pricing. Roof mounting of the air handling unit may be an issue due to the existing solar array, and a structural engineer should be consulted, so consideration for ground or perhaps indoor units (Mech room or interstitial attic) might be an option to explore. Indoor units would require ducted or louvered openings for ventilation air. **EEM 3a is listed as not recommended because the payback is poor.**

EEM-3b: High Efficient RTU with DX Cooling

A high efficient variable volume rooftop unit utilizing electric heating and DX cooling, with energy recovery is evaluated as the proposed replacement system. We have evaluated this system with variable air volume terminal units with electric reheat to allow for zone control and improved comfort conditions. One roof-mounted air handling unit was modeled however in practice this would likely be split into two units to have the Fire Truck bay separate. The temperature and air flow delivered to each space is optimized with reset. Outdoor air is delivered to the spaces as mixed air via the VAV system, so the unit will run continuously during all occupied hours. Energy recovery has been included.

Baseline (Existing) Assumptions:

- Oil fired hot water boiler, 800 mbh heating, 80% efficiency (oversized with system inefficiencies beyond boiler)
- Existing cooling via small through-window and portable A/C units, Cooling Efficiency 11.2 EER (maximum, 9.0 EER average), 11.6 IPLV, Existing

Proposed Assumptions:

- Rooftop unit, DX cooling, electric heating, VAV
- Enthalpy Energy Recovery 60% efficient
- 12,000 CFM, 2,750 CFM OA
- 300 mbh heating, 23 tons cooling
- Improved Efficiency: 12.0 EER, 13.7 IEER, 100% efficient heating (COP 1.0).

		Annual	Electric	Annual	Annual	Annual	Annual	Total	Total		
EEM	Energy Efficiency	Annual	Peak	Electric	#2 Fuel	#2 Fuel	#2 Fuel	Energy	Annual	Estimated	Simple
	Energy Efficiency Measure Description	Electric	Demand	Cost	Oil	Oil	Oil Cost	Consumption	Cost	EEM Cost	Payback
No.	Measure Description	Savings [kWh]	Savings	Savings	Savings	Savings	Savings	Savings	Savings	[\$] (total)	[Years]
		נגאאון	[kW]	[\$]	[gallons]	[mmBtu]	[\$]	[mmBtu]	[\$]		
3b	High Efficient RTU with DX cooling	-93,463	8.82	-\$15,565.50	5,045	706.25	\$7,486.60	387.26	-\$8,078.90	\$160,158.19	-19.8

Table 7: EEM-3b Summary

This option is an improvement over EEM-3a because it is slightly higher in efficiency, includes energy recovery, variable air volume, and better zone control. This option makes sense when some amount of energy efficiency is desirable, without requiring the investment that more extreme measures would involve. Similar to 3a, this measure would require ductwork to extend throughout the space, likely run above ceilings or exposed and ceiling hung. Chases may be necessary to run between floors for the ductwork. Roof mounting may be an issue due to the existing solar array, and a structural engineer should be consulted, so consideration for ground or perhaps indoor units (Mech room or interstitial attic)

might be an option to explore. Indoor units would require ducted or louvered openings for ventilation air. **EEM 3b is listed as not recommended because the payback is poor.**

EEM-3c: High Efficient Heat Pump

A packaged roof-mounted heat pump HVAC unit complete with variable air volume and energy recovery ducted to provide both conditioning and ventilation air. This unit is able to use heat pump technology to provide both heating and cooling, with the heating much more efficient and electric resistance heat.

Baseline (Existing) Assumptions:

- Oil fired hot water boiler, 800 mbh heating, 80% efficiency (oversized with system inefficiencies beyond boiler)
- Existing cooling via small through-window A/C units and various window fans,

Cooling Efficiency 11.2 EER (maximum, 9.0 EER average), 11.6 IPLV, Existing Proposed Assumptions:

Heat pump roof mounted unit, VAV

- Enthalpy Energy Recovery 60% efficient
- 12,000 CFM, 2,750 CFM OA
- 300 mbh heating, 23 tons cooling
- Improved Efficiency: 13.0 EER, 14.2 IEER, 3.4 COP heating

EEM No.	Energy Efficiency Measure Description	Annual Electric Savings [kWh]	Electric Peak Demand Savings [kW]	Annual Electric Cost Savings [\$]	Annual #2 Fuel Oil Savings [gallons]	Annual #2 Fuel Oil Savings [mmBtu]	Savings	Total Energy Consumption Savings [mmBtu]	Total Annual Cost Savings [\$]	Estimated EEM Cost [\$] (total)	Simple Payback [Years]
3c	High Efficient Heat Pump	3,226	10.12	\$537.28	5,045	706.25	\$7,486.60	717.26	\$8,023.88	\$212,902.31	26.5

Table 8: EEM-3c Summary

Heat pumps are generally more than two to three times as efficient as electric resistance, so we would encourage the use of heat pump technology. We'd recommend including energy recovery and variable air volume with terminal units to allow for zone control and improved comfort conditions. Electric reheat in the terminal units would be optional but not included in the calculation. Similar to the code-compliant and better-than-code measures 3a and 3b, this measure would require ductwork to extend throughout the space, likely above the ceiling or exposed and ceiling hung. Chases may be necessary to run between floors. Multiple HPs will likely be utilized if this HVAC system is implemented. This would allow for better control especially since there are two floors and an assembly area with denser occupancy. Roof mounting may be an issue due to the existing solar array, and a structural engineer should be consulted, so consideration for ground or perhaps indoor units (Mech room or interstitial attic) might be an option to explore. Indoor units would require ducted or louvered openings for ventilation air. **EEM 3c is listed as recommended because EEM 3d performs slightly better**, **is better suited to serving the multiple space types and occupancies, and is not expected to be significantly more in cost.**

EEM-3d: VRF System

A VRF system is a variable refrigerant flow system, with distributed indoor units coupled with a modular bank of outdoor condensing style air cooled units, interconnected with small refrigerant piping. The indoor VRF units may be console, wall, or ceiling mounted and may be selected with heat recovery capability. A dedicated outdoor air unit as VRF or heat pump with reversible flow and energy recovery would provide ventilation air to the space. The VRF system performs at a very high efficiency. The calculations include a heat recovery type VRF system.

Baseline (Existing) Assumptions:

- Oil fired hot water boiler, 800 mbh heating, 80% efficiency (oversized with system inefficiencies beyond boiler)
- Existing cooling via small through-window and portable A/C units, Cooling Efficiency 11.2 EER (maximum, 9.0 EER average), 11.6 IPLV,

Proposed Assumptions:

- HP or VRF DOAS with Enthalpy Energy Recovery 60% efficient, 13.0 EER, 14.2 IEER, COP 3.4
- 12,000 CFM, 2,750 CFM OA
- 300 mbh heating, 23 tons cooling
- VRF = 11.2 EER, 17 IEER, COP 3.4

		Ammund	Electric	Annual	Annual	Annual	Annual	Total	Total		
		Annual	Peak	Electric	#2 Fuel	#2 Fuel	#2 Fuel	Energy	Annual	Estimated	Simple
EEN	- 57 7	Electric	Demand	Cost	Oil	Oil	Oil Cost	Consumption	Cost	EEM Cost	Payback
No.	Measure Description	Savings	Savings	Savings	Savings	Savings	Savings	Savings	Savings	[\$] (total)	[Years]
		[kWh]	[kW]	[\$]	[gallons]	[mmBtu]	[\$]	[mmBtu]	[\$]		
3d	VRF System	5,067	12.53	\$843.84	5,045	706.25	\$7,486.60	723.54	\$8,330.44	\$240,506.34	28.9

Table 9: EEM-3d Summary

The benefit of the VRF system is that the piping is small, units are very quiet, easily located and mounted, the system is modular in nature providing for great comfort control and redundancy, has energy sharing capabilities to optimize performance, and ventilation may be provided by a demand controlled dedicated ventilation unit with energy recovery this would allow for small ductwork and precise control to avoid under or over ventilating. Roof mounted condensing equipment would be relatively compact and could be located at grade if the existing solar array does not afford any pace under or beside the panels. Panels could be elevated somewhat to accommodate the condensing unit. The dedicated ventilation unit would be relatively small and similarly could be placed on the roof or indoor in the mechanical room or in the interstitial attic space. **EEM 3d is listed as recommended due to its energy and carbon reduction, flexibility and versatility.** This type of system does require careful selection and design and a contractor certified by the manufacturer to ensure the systems operate at low temperatures and in the desired conditions.

EEM-3e: Geothermal System

A geothermal heat pump system utilizes a geo-exchange well field coupled with extended range water source heat pump type units to efficiently provide space conditioning. The indoor units contain compressors, which extract energy from the attached water loop to condition the air. The water loop is pumped through underground vertical wells, and use the naturally constant ground temperature of the earth as both a heat source and sink as needed. To a greater degree than a VRF system, this system allows for sharing of energy throughout a water heat pump loop.

Baseline (Existing) Assumptions:

- Oil fired hot water boiler, 800 mbh heating, 80% efficiency (oversized with system inefficiencies beyond boiler)
- Existing cooling via small through-window and portable A/C units, Cooling Efficiency 11.2 EER (maximum, 9.0 EER average), 11.6 IPLV

Proposed Assumptions:

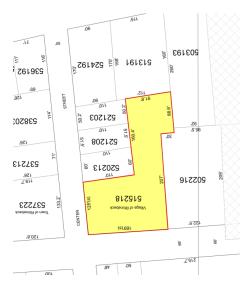
- Geothermal heat pump AHU, VAV
- Enthalpy Energy Recovery 60% efficient
- 12,000 CFM, 2,750 CFM OA
- 300 mbh heating, 23 tons cooling
- 18.1 EER, 3.6 COP
- 19 W/gpm loop pumps

Table 10: EEM-3e Summary

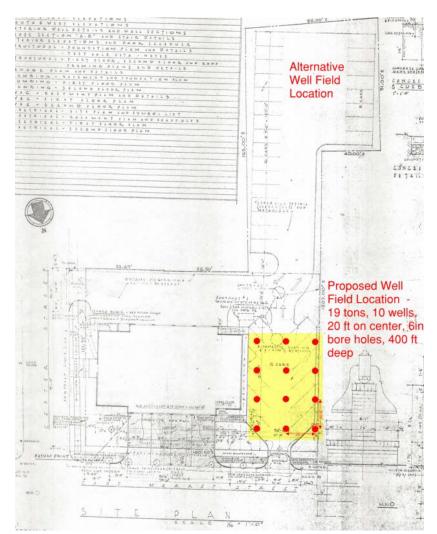
		Annual	Electric	Annual	Annual	Annual	Annual	Total	Total		
	Energy Efficiency	Annual	Peak	Electric	#2 Fuel	#2 Fuel	#2 Fuel	Energy	Annual	Estimated	Simple
EEM	- 37 7	Electric	Demand	Cost	Oil	Oil	Oil Cost	Consumption	Cost	EEM Cost	Payback
No.	Measure Description	Savings	Savings	Savings	Savings	Savings	Savings	Savings	Savings	[\$] (total)	[Years]
		[kWh]	[kW]	[\$]	[gallons]	[mmBtu]	[\$]	[mmBtu]	[\$]		
3e	Geothermal System	6,144	10.09	\$1,023.20	5,045	706.25	\$7,486.60	727.22	\$8,509.80	\$487,178.33	57.2

A location for the well field will need to be determined. An open green space is usually the best option because there is some horizontal piping required to connect to the vertical wells. However an area under a parking lot is acceptable as well. The downside of using a parking lot is likely and increase in restoration costs. Coordination cost with drainage piping, and utility lines will also be required. The spacing of the wells generally is 20 feet on center, with 400 feet deep wells and 6 inches diameter bores. A 48-hour test well is recommended to confirm ground composition and thermal conductivity. Shallower sample borings can be performed but this information generally only offers depth of casing needed (depth of loose soil to bedrock). There is a higher upfront cost of a geothermal system, with a large portion of the costs in the well field. Once the system is in place, the maintenance costs are relatively low as the underground piping does not have any moving parts requiring maintenance. **EEM 3e is listed as not recommended, due to a high first cost when incentives are not considered.**





Tax Parcel



Site Plan

EEM-4: DOMESTIC HOT WATER REPLACEMENT

The existing electric domestic water heaters are to be replaced. Four (4) options were evaluated according to the HVAC system upgrades:

EEM-4a - DHW Propane Fired Unit EEM-4b - Electric Water Unit EEM-4c - DHW Air Source Heat Pump EEM-4d - Geothermal Heat Pump Unit

Fixtures may be upgraded to water saving type, however due to the use, there is limited benefit and this has not been evaluated separately.

EEM-4a: DHW Propane Fired Unit

Tank type semi-instantaneous propane fired water heaters were evaluated. This is a traditional system that is generally cost-effective.

Baseline (Existing) Assumptions:

- 32E oil-fired 32 gallon tank type water heater, 80% efficiency, 0.62 Uniform Energy Factor
- 2x66 gallon electric water heater manufactured by Bock, 0.84 Uniform Energy Factor Proposed Assumptions:
 - Office : Three 50 gallon, propane fired, tank type water heater 92% efficiency

Table 11: EEM-4a Summary

EEM No.	Energy Efficiency Measure Description	Annual Electric Savings [kWh]	Electric Peak Demand Savings [kW]	Savings	Annual Fossil Fuel Savings [gallons]	Annual Fossil Fuel Savings [mmBtu]	Savings	Total Energy Consumption Savings [mmBtu]	Total Annual Cost Savings [\$]	Estimated EEM Cost [\$] (total)	Simple Payback [Years]
4a	DHW Propane Fired Unit	7,676	0.17	\$1,278.44	-48	0.70	-\$233.95	26.90	\$1,044.48	\$10,740.00	10.3

This measure provides some energy savings, but is not recommended due to the lengthy payback.

EEM-4b: DHW Electric Unit

Tank type semi-instantaneous electric water heaters were evaluated.

Baseline (Existing) Assumptions:

- 32E oil-fired 32 gallon tank type water heater, 80% efficiency, 0.62 Uniform Energy Factor
- 2x66 gallon electric water heater manufactured by Bock 0.84 Uniform Energy Factor
- Proposed Assumptions:
 - Office : Three 50 gallon, electric tank type water heaters , 0.92 Uniform Energy Factor, COP 1.0

		Annual	Electric	Annual	Annual	Annual	Annual	Total	Total		
EEM	Energy Efficiency	Annual	Peak	Electric	#2 Fuel	#2 Fuel	#2 Fuel	Energy	Annual	Estimated	Simple
No.	Energy Efficiency Measure Description	Electric	Demand	Cost	Oil	Oil	Oil Cost	Consumption	Cost	EEM Cost	Payback
INO.	Measure Description	Savings	Savings	Savings	Savings	Savings	Savings	Savings	Savings	[\$] (total)	[Years]
		[kWh]	[kW]	[\$]	[gallons]	[mmBtu]	[\$]	[mmBtu]	[\$]		
4b	DHW Electric Unit	224	0.04	\$37.27	120	16.76	\$177.69	17.53	\$214.96	\$9,240.00	43.0

Table 12: EEM-4b Summary

This measure provides some energy savings, but is not recommended due to the limited energy benefit and lengthy payback.

EEM-4c: DHW Air Source Heat Pump

The existing water heaters are to be replaced with air source heat pump water heaters. ASHP water heaters use electricity to move heat from one place to another instead of generating heat directly, therefore they can be two or three times more energy efficient than conventional water heaters. Because these units extract energy from the ambient air they require a room of sufficient size to extract the heat from. In general rooms of sufficient size below grade are often the preferred installation location.

Baseline (Existing) Assumptions:

- 32E oil-fired 32 gallon tank type water heater, 80% efficiency, 0.62 Uniform Energy Factor
- 2x66 gallon electric water heater manufactured by Bock 0.84 Uniform Energy Factor

Proposed Assumptions:

• Office : Three 50 gallon, air source heat pump, tank type domestic water heaters, Uniform Energy Factor of 2.5, HSPF 8.2

EEM No.	Energy Efficiency Measure Description	Annual Electric Savings [kWh]	Electric Peak Demand Savings [kW]	Annual Electric Cost Savings [\$]	Annual #2 Fuel Oil Savings [gallons]	Annual #2 Fuel Oil Savings [mmBtu]	Annual #2 Fuel Oil Cost Savings [\$]	Total Energy Consumption Savings [mmBtu]	Total Annual Cost Savings [\$]	Estimated EEM Cost [\$] (total)	Simple Payback [Years]
4c	DHW Air Source Heat Pump	5,019	0.06	\$835.90	120	16.76	\$177.69	33.89	\$1,013.59	\$16,224.00	16.0

Table 13: EEM-4c Summary

The air source heat pump water heaters would need to be located inside and in an area that can maintain 40° or higher because they do not operate at optimal efficiency when in a colder area. This measure is recommended, as the simple payback is reasonable.

EEM-4d: DHW Geothermal Well Field

The existing water heaters are to be replaced with a connection to a geothermal well field. This option would be a water to water heat pump and tank option.

Baseline (Existing) Assumptions:

 32E oil-fired 32 gallon tank type water heater, 80% efficiency, 0.62 Uniform Energy Factor

• 2x66 gallon electric water heater manufactured by Bock 0.84 Uniform Energy Factor Proposed Assumptions:

• Office : Three 50 gallon, domestic water heater, Uniform energy factor of 3.0, connected to the well field, HSPF 9.6

EEM No.	Energy Efficiency Measure Description	Annual Electric Savings [kWh]	Demand	Annual Electric Cost Savings [\$]	Annual #2 Fuel Oil Savings [gallons]	Annual #2 Fuel Oil Savings [mmBtu]	Annual #2 Fuel Oil Cost Savings [\$]	Total Energy Consumption Savings [mmBtu]	Total Annual Cost Savings [\$]	Estimated EEM Cost [\$] (total)	Simple Payback [Years]
4d	DHW Geothermal Well Field	5,603	0.07	\$933.13	120	16.76	\$177.69	35.89	\$1,110.82	\$19,224.00	17.3

Table 14: EEM-4d Summary

This system would be connected to the HVAC system geothermal loop with a water to domestic water heat pump. The ground source heat pumps selected would be constructed for potable water use and separate the ground loop from the domestic water loop. This measures is listed as recommended nonenergy reasons since it relies on the HVAC geothermal option being selected. This measure saves slightly more energy than EEM 4c ASHP water heater, is a slightly longer payback, and has slightly higher first cost when incentives are not considered.

EEM-5: APPLIANCE REPLACEMENT AND HOOD CONTROLS

The existing appliances in the office/kitchen area may be replaced with ENERGY Star certified appliances. This would create a reduction in plug loads. Kitchen demand control ventilation would also be provided. This would be tied into a hood control module, which determines the need for exhaust based on smoke and temperature beneath the kitchen hood via hood smoke and temperature sensors. The controls would be linked to the system fans, modulating as needed. Energy is saved by reduced fan power at the supply and exhaust fans, from the reduced airflow, reduced operating hours, as well as the reduction of outdoor air requiring conditioning.

Baseline Assumptions:

- Existing appliances
- Four (4) refrigerators, US Federal Standard efficiency
- One(1) Ice Maker, US Federal Standard efficiency
- No heat/smoke control present

Proposed Assumptions:

- ENERGY Star Appliances
- Four (4) refrigerators, ENERGY Star efficiency
- One (1) Ice Maker, ENERGY Star efficiency
- Heat/smoke controlled kitchen hood

		Annual	Electric	Annual	Annual	Annual	Annual	Total	Total		
EEM	Energy Efficiency	Annual	Peak	Electric	#2 Fuel	#2 Fuel	#2 Fuel	Energy	Annual	Estimated	Simple
	Energy Efficiency Measure Description	Electric	Demand	Cost	Oil	Oil	Oil Cost	Consumption	Cost	EEM Cost	Payback
No.	Measure Description	Savings	Savings	Savings	Savings	Savings	Savings	Savings	Savings	[\$] (total)	[Years]
		[kWh]	[kW]	[\$]	[gallons]	[mmBtu]	[\$]	[mmBtu]	[\$]		
5	Appliance Replacement	6,026	1.02	\$1,003.51	163	22.75	\$241.18	43.32	\$1,244.69	\$15,427.00	12.4

Table 13: EEM-5 Summary

This measure with appliance replacement and integration of kitchen hood controls is recommended because the simple payback is less than the expected useful life of the systems. However, if the kitchen hood is rarely used, the benefit might in reality be limited.

CONCLUSION

Based on the findings of the study, we recommend pursing energy efficiency measures EEM 1 highefficiency lighting, EEM 2 addressing air infiltration, EEM3 selecting an HVAC system upgrade 3d, EEM 4 selecting a domestic hot water system upgrade from 4c, and EEM 5 appliance replacement and hood heat/smoke control. We also encourage leveraging the various incentive program available however these incentive programs are not guaranteed, are subject to change, and are contingent on program acceptance, eligibility, and available funding. These measures will help improve the efficiency of building, reduce the carbon footprint and have a positive impact on the occupants of your facility and the environment. We hope the findings of this report will assist you in making decisions about energy efficiency improvements in your facility.

ADDITIONAL CONSIDERATIONS

Although the main considerations in selecting an HVAC system are typically energy and cost implications, there are several other factors at play.

Existing Useful Life of Equipment

A full life cycle cost analysis has not been performed as part of this study. However, each system has a different lifespan. For example, a rooftop unit has an expected useful life of 20 years before replacement becomes necessary, while a heat pump can be expected to last 25 years.

	Expe	cted Useful Life	
Equipment Description	Years	Equipment Description	Years
DX Rooftop Unit	20	Fossil Fuel DWH	15
Envelope Improvements	30	ASHP DHW	20
Heat Pump	25	VRF	25
Fossil Fuel Boiler	25	Pumps	15
Energy Star Appliances	14		

In order to fully capture the replacement and the true cost of each system type, a full life cycle cost analysis may be warranted.

Carbon Reduction

Much of the motivation to reduce fossil fuel usage is to address climate change by reducing carbon and greenhouse gas emissions. New York State currently has one of the cleanest electric grids in the nation, and has goals of 1000% zero emission electricity by 2040. However, today natural gas still remains slightly less carbon intensive per unit of energy than electricity, due to the fossil fuels required to produce and distribute electricity, which is often counter-intuitive. With the New York's focus on renewable energy, that is likely to change, especially over the lifespan of equipment with long expected life.

Gr	reenhouse Gas	Emissions	
Tog	Carbon	Saving Base	
Tag	Consumption	Consun	nption
	(mt CO ₂ e)	(mt CO ₂ e)	(%)
BASELINE	63.0		
EEM- 1	56.6	6.4	10.1%
EEM- 2	53.5	9.5	15.0%
EEM-3A	87.4	-24.4	-38.7%
EEM-3B	72.2	-9.2	-14.6%
EEM-3C	23.8	39.2	62.2%
EEM-3D	22.9	40.1	63.6%
EEM-3E	22.4	40.6	64.5%
EEM-4A	59.5	3.5	5.5%
EEM-4B	59.6	3.4	5.4%
EEM-4C	59.3	3.7	5.9%
EEM-5	58.7	4.2	6.7%

Utility Cost Inflation

New York State has aggressive carbon-reduction goals, which require the electrification of heating systems to succeed. One method of encouraging the switch from fossil fuels to electric heating in our climate is to provide financial incentives and penalties. Already, NYSERDA and the major utility companies have incentive programs to mitigate first costs. In the future, the economic incentives may migrate to utility rates themselves, in the form of electric rate subsidies or carbon taxes. For example, in 2018, Canada implemented a carbon tax based on consumption meant to penalize excessive fossil fuel use. While the future of energy is unknown, it is a possibility to consider.

Additional Energy Efficiency Measures

When designing a high-efficiency HVAC system with a high first cost, such as a high-efficiency ground source heat pump system, it is important to include a range of additional energy efficiency measures. If the load of the HVAC system can be reduced, so can the equipment size, which decreases the cost premium required for the high-efficiency option. It is encouraged to include as many energy efficiency measures as feasible to ensure both a high-performing building as well as to mitigate some of the equipment costs. At the current design phase, due to the level of detail, not all of these energy efficiency measures can be captured or are even known, and the interactive effects have not been accounted for in this report.

The following potential measures were identified during the site visit, but were not studied as part of this project.

- Additional Photovoltaic
- Additional electric vehicle charging stations
- Upgrade of compressed air systems with premium equipment with possible energy recovery

Project Stage

This project is in the study phase and as such, many assumptions and generalizations were made in the analyses. It is prudent to make conservative assumptions in order to avoid overstating energy savings or cost implications. As the design progresses, the models may be refined, and typically more energy savings are demonstrated.

CALCULATIONS

All calculations generally follow NYS 8.0 Technical Resource Manual methods, unless noted.

Awn a 9800 a </th <th>EEM-1 : Lighting closest TRM location Poughkeepsie</th> <th></th> <th>Office Areas</th> <th></th>	EEM-1 : Lighting closest TRM location Poughkeepsie		Office Areas															
AMM - - MSR W 1000 /k 1988.58 x/l 1 + 0.066 Types difficul LPD (ASHRAE 90.12016 430%, imponenter) 0.05 Wirt 0.05 Wirt - - 4394.0 / 1000 /k 1 + HVAC, /k CF HVAC, 0.066 0.047 - 1.015 X/l Wom - 4394.0 / 1000 /k 1 + HVAC, /k 0.02 MCAC, 0.002 0.002 0.002 0.002 0.002 0.002 - 4394.0 / 1000 x 1988.58 x 4.002 - 4394.0 / 1000 x 188.58 x 4.002 - 4394.0 / 1000 x 188.58 x 4.002 - 4.002 x 188.58 x 4.002 - 4.002 x 188.58 x 4.002 - 4.002 x 4.002 x 4.002 x 4.002 x 4.002 x 4.002 x 4.002			ΔkWh	=	units	x((W _{base}	-	Wee)/	1000)x	hrson	x(1	+	HVAC _c)
AWN $=$ 9806 Number of the AMR 10, 120 4-30%, imposement) 0.5% With Interfor AMR 45, 01 2016 430%, imposement) 0.5% With ΔWW $=$ MW $=$ W V 1000 V_1 1 $+$ VAC_0 V 1000 V_1 1 $+$ VAC_0 V V 1000 V_1 1 $+$ VAC_0 V	Office Areas		ΔkWh	=				-)/		,	1988.58		1	+	-	ý
$ \begin{array}{c} \text{Market house from TRM, reduce to account for Tam-dom 1 1985, 59 hours } \\ \text{MAC}, & \text{OBSE} & \text{AWW} & = & 1 \\ \text{MAC}, & \text{OBSE} & \text{AWW} & = & 5.001 \\ \text{MAC}, & \text{ODSE} & \text{AWW} & = & 5.001 \\ \text{MAC}, & \text{ODSE} & \text{AWW} & = & 5.001 \\ \text{MAC}, & \text{ODSE} & \text{AWW} & = & 5.001 \\ Constraints produce to constraints of the second to the second to$			ΔkWh	=	9806	, iii				,		,						,
HVACp: 0.066 ΔWV = 1 X(V) 902.0 - 438.0 y 1000 y(I) 1 + 0.75 yz 0.02 HVACp: 0.000 453.0 MMBPU - mills x(Wacs - Wac y 1000 x hrss x HVACp - Wacs - Wacs y 1000 x hrss x HVACp - Wacs y 1000 x hrss x HVACp - Wacs - Wacs y 1000 x hrss x HVACp - - 494.0 y 1000 x hrss x HVACp - - - 494.0 y 1000 x hrss<		0.55 W/sf																
$\begin{split} & \text{HVAC}, & 0.066 & \Delta W & = 1 \\ & \text{HVAC}, & 0.007 & \text{AW} & = 5.001 \\ & \text{HVAC}, & 0.007 & \text{AW} & = 5.001 \\ & \text{HVAC}, & 0.007 & \text{AW} & = 5.001 \\ & \text{HVAC}, & 0.007 & \text{AW} & = 5.001 \\ & \text{HVAC}, & 0.007 & \text{AW} & \text{AW} & 0.007 & \text{AW} & \text{AW} & \text{AW} & 0.007 & \text{AW} & \text{AW} & \text{AW} & \text{AW} & 0.007 & \text{AW} & $	Interior hours from TRM, reduce to account for 10am-4pm	1988.58 hours	ΔkW	=	units	x((W _{base}	-	Wee)/	1000)x(1	+	HVAC _d)x	CF	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	HVAC _c	0.066	ΔkW	=	1	x((-)/	1000)x(1	+	0.175)x	0.92	
Office wattage 10 mode wattage	HVACd	0.175	ΔkW	=	5.001							, ,						
Office wattage +10% credit for OS Controls 434 W - 1 x(902.0. - 4394.0 y 1000 x 1988.58 x -0.02 Assumed wattage/st based on site wist obsensions 1.1 W/M	HVAC _{ff}	-0.002																
Office wattage + 10% credit for QS Controls 444MBtu * 1 V 902.0 - 4394.0 V 1000 x 1988.58 x - 0.02 Assumed wattage f based on site wist dosenations 1.1 W/M = - 133 V 902.0 - 4394.0 V 1000 x 1988.58 x - 0.02 So of dice 2000 F Filtratuck Storage - W/M = - - V V 1000 x 1886.58 x -	Office wattage	4535 W	ΔMMBtu	=	units	x(W _{base}	-	Wee)/	1000	х	hrs	х	HVAC _{ff}			
Assumed wattage of based on site visit observations 1.1 W/sf and the served of th	Office wattage +10% credit for OS Controls	4394 W`	ΔMMBtu	=	1	x(-)/	1000	х	1988.58	х	-0.002			
SF of office $\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	Existing:		ΔMMBtu	=	-18													
baseline wattage basel	Assumed wattage/sf based on site visit observations	1.1 W/sf	ΔFuel Oil	=	-131													
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	SF of office	8200 SF																
$\frac{AkWh = 1}{AkWh = 4029}$ $\frac{AkWh = 1}{AkW = 4029}$ $\frac{AkWh = 4029}{AkW = 4029}$ $\frac{AkW = 4029}{AkW = 4029}$ $\frac{AkW = 4029}{AkW = 4029}$ $\frac{AkW = 4029}{AkW = 1}$ $\frac{AkW = 4029}{AkW = 2.131}$ $\frac{AkW = 4.13}{AkW = 4.13}$ $AkW = 4.13$	baseline wattage	9020 W	Firetruck Storage															
Linetrock Storage / MaintananceProposed : Proposed : Typical Aud/Pire Station Avg (ASHRAE 90.1 2016 +30% improvement)0.37 W/sfAkW = 4029Number of the station Avg (ASHRAE 90.1 2016 +30% improvement)0.37 W/sfAkW = units AkW = 1x((Wase - Wase / 1000)x(1+ 	LPD with 10% credit for OS Controls	0.50 W/sf	ΔkWh	=	units	x((W _{base}	-	Wee)/)x		x(1	+)
Proposed : Typical Atur/Fire Station Arg (ASHRAE 90.12016 +30% improvement)0.37 W/sf 1884.6 hours $\Delta kW = units \\ \Delta kW = 1 \\ 1 \\ KW = 2.131 \\ KW =$			ΔkWh	=	1	x((3240.0	-	1202.0)/	1000)x	1854.6	x(1	+	0.066)
Typical Auto/Fire Station Ayg (ASHRAE 90.1 2016 + 30% improvement) 0.37 W/sf ΔkW = units x((Wbase - Wee y 1000 y(1 + HVAC_d y CF nterior hours from TRM, reduce to account for 10am 4pm 1884.6 hours ΔkW = 1 x((3240.0 - 1202.0 y 1000 yx(1 + HVAC_d yx CF HVAC_1 0.066 ΔkW = 2.131 - X(U 3240.0 - 1202.0 y 1000 x hrs x HVAC_d yx 0.89 HVAC_2 0.075 - 1202.0 y 1000 x hrs x HVAC_fr - - Wee y 1000 x hrs x HVAC_fr - - - Wee y 1000 x hrs x HVAC_fr - - - Wee y 1000 x hrs x HVAC_fr - - - - 1000 y hrs<	Firetruck Storage/ Maintenance		ΔkWh	=	4029													
$\frac{\Delta kW}{\mu + \Delta C_{c}} = 1 \\ \frac{\Delta kW}{\mu} = 2.33 \\ \frac{\Delta kW}{\mu} =$	•																	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Typical Auto/Fire Station Avg (ASHRAE 90.1 2016 +30% improvement)	0.37 W/sf	ΔkW	=	units	x((-		,			1	+	HVAC _d)x		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Interior hours from TRM, reduce to account for 10am-4pm	1854.6 hours	ΔkW	=	1	×((3240.0	-	1202.0)/	1000)x(1	+	0.175)x	0.89	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	HVAC _c	0.066	ΔkW	=	2.131													
Maintenace wattage 1336 W $\Delta MMBtu = 1$ x 3240.0 - 1202.0 y 1000 x 1854.6 x 0.00 Maintenace wattage +10% credit for OS Controls 1202 W $\Delta MMBtu = -8$ Existing: Assumed wattage/sf based on site visit observations 0.9 W/sf SF of firetruck storage 3600 SF Exterior baseline wattage 0 3240 W $\Delta kWh = units x((W_{base} - W_{ee})/1000) x hrs_{op} x(1 + HVAC_{c}) x LP With 10% credit for OS Controls 0.33 W/sf \Delta kWh = 1 x((900.0 - 324.0 y) 1000) x 2.891 x(1 + 0 \Delta kWh = 1665Exterior Proposed :6x Building Mounted, 54W each 2.891 hours \Delta kW = 0.576Existing:Exterior Hours, reduced 2.891 hours \Delta kWh = 15500Total \Delta kWh = 15500Total \Delta kWh = 52.581.46$	HVACd	0.175																
Maintenace wattage +10% credit for OS Controls 1202 W' $\frac{\Delta MMBtu = -8}{\Delta Fuel O(l = -54}$ Assumed wattage/sf based on site visit observations 0.9 W/sf SF of firstruck storage 3600 SF $\frac{Extarior}{2,891 \text{ with } 0.33 \text{ W/sf}} = \text{units } x((W_{base} - W_{ee})/ 1000)x \text{ hrs}_{op} x(1 + HVAC_{c})x CF$ baseline wattage (19% credit for OS Controls 0.33 W/sf $\Delta kWh = 1 x((900.0 - 324.0)/ 1000)x (1 + HVAC_{d})x CF$ $\frac{\Delta kW}{2} = \text{units } x((W_{base} - W_{ee})/ 1000)x(1 + HVAC_{d})x CF$ for Building Mounted, 54W each 2,891 hours $\Delta kW = 1 x((900.0 - 324.0)/ 1000)x(1 + 0)x 1$ Exterior Hours, reduced 2,891 hours $\Delta kW = 1 x((900.0 - 324.0)/ 1000)x(1 + 0)x 1$ Exterior Hours, reduced 2,891 hours $\Delta kW = 1 x((900.0 - 324.0)/ 1000)x(1 + 0)x 1$ Exterior Hours, reduced 2,891 hours $\Delta kW = 1 x((900.0 - 324.0)/ 1000)x(1 + 0)x 1$ Exterior Hours, reduced 2,891 hours $\Delta kW = 1 x((900.0 - 324.0)/ 1000)x(1 + 0)x 1$ Extended the second sec	HVAC _{ff}	-0.002	ΔMMBtu	=	units	x(W _{base}	-	Wee)/	1000	х	hrs	х	HVAC _{ff}			
$\Delta Fuel Oil = -54$ Assumed wattage/s based on site visit observations0.9 W/sfSF of firetruck storage3600 SFExterior3240 WDasaline wattage0.33 W/sfLPD with 10% credit for OS Controls0.33 W/sf $\Delta kWh = 1$ x((900.0 - 324.0)/ 1000)x $kWh = 1665$ ExteriorProposed : $\Delta kW = 1$ $\alpha kW = 1$ x((900.0 - 324.0)/ 1000)x(1 + HVAC_d) x $cF k Building Mounted, 54W each2,891 hours\Delta kW = 1ch kW = 1ch kW = 0.576ch kW = 15500for bluiding Mounted, 150W each900 WTotal \Delta kWh = 15500Total \Delta kWh = 7.71Total \Delta kWh = 82,581.46$	Maintenace wattage	1336 W	ΔMMBtu	=	1	x(3240.0	-	1202.0)/	1000	х	1854.6	х	0.00			
Assumed wattage/sf based on site visit observations 0.9 W/sf SF of firetruck storage 3600 SF Exterior baseline wattage 3240 W $\Delta kWh = units x((W_{base} - W_{ee})/1000)x hrs_{op} x(1 + HVAC_{c})x LPD with 10% credit for OS Controls 0.3 W/sf \Delta kWh = 1 x((90.0 - 324.0)/1000)x 2,891 x(1 + HVAC_{d})x CFExteriorProposed :6x Building Mounted, 54W each 324 W \Delta kW = 1 x((90.0 - 324.0)/1000)x(1 + HVAC_{d})x CFExterior Hours, reduced 2,891 hours \Delta kW = 0.576Exterior Hours, reduced 900 W Total \Delta kWh = 15500Total \Delta kWh = 15500Total \Delta kWh = 125,811.46$	Maintenace wattage +10% credit for OS Controls	1202 W`	ΔMMBtu	=														
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Existing:		ΔFuel Oil	=	-54													
baseline wattage 3240 W $\Delta kWh = units x((W_{base} - W_{ee})/ 1000)x hrs_{op} x(1 + HVAC_{c}) + HVAC_{c}$ LPD with 10% credit for OS Controls 0.33 W/sf $\Delta kWh = 1$ x((900.0 - 324.0)/ 1000)x 2,891 x(1 + 0 + 1000) + 2,891 x(1 + 0 + 1000)	Assumed wattage/sf based on site visit observations	0.9 W/sf																
LPD with 10% credit for OS Controls 0.33 W/sf $\Delta kWh = 1$ x(() 900.0 - 324.0)/ 1000)x 2,891 x() 1 + 0 Exterior Proposed : $\Delta kWh = 1665$ $\Delta kW = 1$ x(() $\Psi_{base} - \Psi_{ee}$)/ 1000)x() 1 + HVAC _d)x CF 6x Building Mounted, 54W each 324 W $\Delta kW = 1$ x(() 900.0 - 324.0)/ 1000)x() 1 + 0)x 1 Exterior Hours, reduced 2,891 hours $\Delta kW = 0.576$ x(() 900.0 - 324.0)/ 1000)x() 1 + 0)x 1 Exterior Hours, reduced 2,891 hours $\Delta kWh = 15500$ Total $\Delta kW = 7.711$ Total $\Delta kW = 7.711$ Total $\Delta kW = 7.711$ Total $\Delta kWh = 7.711$ $\Delta kWh = 32,581.46$ V V	SF of firetruck storage	3600 SF	Exterior															
$ \begin{array}{c} \Delta kWh = 1665 \\ \hline \\ Proposed: \\ 6x Building Mounted, 54W each \\ Sterior Hours, reduced \\ Existing: \\ 6x Building Mounted, 150W each \\ \hline \\ Building Mounted, 150W each \\ \hline \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ $	baseline wattage	3240 W	ΔkWh	=	units	x((W _{base}	-	Wee	,	1000		hrs _{op}		1	+	HVAC _c)
ExteriorProposed : $\Delta kW = units x((W_{base} - W_{ee})/ 1000)x(1 + HVAC_d)x CF$ 6x Building Mounted, 54W each324 W $\Delta kW = 1 x((900.0 - 324.0)/ 1000)x(1 + 0)x 1$ Exterior Hours, reduced2,891 hours $\Delta kW = 0.576$ Existing:Existing:6x Building Mounted, 150W each900 WTotal $\Delta kWh = 15500$ Total $\Delta kW = 7.71$ Total $\Delta kWh = -185.411$ $\Delta kWh = $2,581.46$	LPD with 10% credit for OS Controls	0.33 W/sf		=		x((900.0	-	324.0)/	1000)x	2,891	x(1	+	0)
Proposed : ΔkW =unitsx((Wbase-Wee//1000)x(1+HVACd)xCF6x Building Mounted, 54W each324 W ΔkW =1x((900.0-324.0)/1000)x(1+0)x1Exterior Hours, reduced2,891 hours ΔkW =0.576Existing:Total ΔkWh =155006x Building Mounted, 150W each900 WTotal ΔkWh =7.71Total $\Delta fuel Oil$ =-185.411 $\Delta k Wh$ =\$2,581.46			ΔkWh	=	1665													
6x Building Mounted, 54W each 324 W ΔkW = 1 x((900.0 - 324.0)/ 1000)x(1 + 0)x 1 Exterior Hours, reduced 2,891 hours ΔkW = 0.576 Existing:	Exterior																	
Exterior Hours, reduced 2,891 hours ΔkW = 0.576 Existing:	•		ΔkW	=	units	x((-		,			1	+	HVAC _d)x	CF	
Existing: 900 W Total ΔkWh = 15500 6x Building Mounted, 150W each 900 W Total ΔkW = 7.71 Total ΔkW = 7.71 Total ΔkWh = -185.411 Δ\$ kWh = \$2,581.46				=		×((900.0	-	324.0)/	1000)x(1	+	0)x	1	
6x Building Mounted, 150W each 900 W Total ΔkWh = 15500 Total ΔkW = 7.71 Total Δfuel Oil = -185.411 Δ\$ kWh = \$2,581.46	Exterior Hours, reduced	2,891 hours	ΔkW	=	0.576													
$Total \Delta kW = 7.71 Total \Delta fuel Oil = -185.411 \Delta$ kWh = $2,581.46$						_												
Total Δfuel Oil = -185.411 Δ\$ kWh = \$2,581.46	6x Building Mounted, 150W each	900 W																
$\Delta \$ kWh = \$2,581.46$																		
						_												
	none (20		Δ\$ kWh Δ\$ fuel oil	=	\$2,581.46 (\$275.16)	-												

EEM-2: Envelope Improvements																						
Room Temp Setpoint Cooling	75 °F																					
OA Temp Setpoint Cooling	89 °F	Roof																				
Room Temp Setpoint Heating	70 °F	∆kWh _a	=(((Roof Uvalue _{base}	х	Roof SF _{base})-(Roof Uvalue _{ee}	х	Roof SF _{ee}))x(Toutdoor, design	-	Tindoor, setpoint)/	1000)x	EFLH _{cool}	/	IPLV		
OA Temp Setpoint Heating	0 °F	∆kWh _a	=(((0.077	х	5400)-(0.033	х	5400))x(89	-	75)/	1000)x	576	/	11.6		
		ΔkWh_a	=	163																		
EFLH Cooling and Heating, Poughkeepsie																						
Small Office/Auto , Cooling	575.5 EFLH _{cool}	∆kWh _{cool}	=	163	T																	
Small Office/Auto , Heating	1616 EFLH _{beat}	-			-																	
page 926		∆kWh _a	=(((Roof Uvalue _{base}	х	Roof SF _{base})-(Roof Uvalueee	х	Roof SFee))x(Tindoor, setpoint	-	Toutdoor, design)/	1000)x	EFLHheat	/	COPx3.412		
		∆kWh _a	=(((0.077	х	5400)-(0.033	x	5400))x(-	0)/	1000)x	1616	/	68.24		
		∆kWh _a	=	390			,,				<i>"</i> (<i>,</i>		,					
		a																				
		∆kWh _{heat}	=	390	T	No Electric Hea	at. but s	slight pumping p	ower	(converted bi	tu and	HP to COP)										
					-			5 1 1 51				,										
		ΔkW_a	=(((Roof Uvalue _{base}	х	Roof SF _{base})-(Roof Uvalue _{ee}	х	Roof SF _{ee}))x(Toutdoor, design	-	Tindoor, setpoint)/	1000)/	EER				
		ΔkWa	=(((0.077	х	5400)-(0.033	х	5400))x(89	-	75)/	1000)/	9.0				
		ΔkWa	=	0.366			,,,				,, (,		,					
Roof		a																				
Roof SF	5400 SF	∆kW _{cool}	=	0.366	Т																	
Existing: Built-Up roofing, no insulation R=13	0.077 U	L			-																	
New: 6" Insulation, R=5/in, R-30 total	0.033 U	ΔkW_a	=(((Roof Uvalue _{base}	х	Roof SF _{base})-(Roof Uvalue _{ee}	х	Roof SF _{ee}))x(Toutdoor, design	-	Tindoor, setpoint)/	1000)/	COPx3.412				
Cooling Efficiency (Existing wall a/c 9,000 btu, 11.2 EER max, use avg)	9 EER	ΔkWa	=(((0.077	х	5400)-(0.033	х	5400))x(-	75)/	1000)/	68.2				
Cooling Efficiency, existing average	11.6 IPLV	ΔkWa	=	0.048			,,,				,, (,		,					
Heating Elec Efficiency (Suppl. heat from plug in and A/C, assume 10%)	2.5 COP	a																				
Heating Fuel Efficiency (existing boiler)	80% Eff	∆kW _{heat}	=	0.048	T	No Electric Hea	at. but s	slight pumping p	ower	(converted bi	tu and	HP to COP)										
5 · · · · · · · · · · · · · · · · · · ·		licut			-			5 1 1 1 9 P		,		/ /										
		∆MMbtu _a	=(((Roof Uvalue _{base}	х	Roof SF _{base})-(Roof Uvalue _{ee}	x	Roof SF _{ee}))x(Tindoor, setpoint	-	Toutdoor, design)/	1000)x	EFLHheat	/	Eff _{FuelHeat}	/	1000
		∆MMbtu _a	=(((0.077	х	5400)-(0.033	x	5400))x(-	0)/	1000)x	1616	/	80%	/	1000
															,		,					

			_
ΔMMBtu	=	33.273	
∆ Fuel Oil	=	238	
			_
Total ∆kWh	=	163	T
Total ∆kW	=	0.414	
∆ Fuel Oil	=	238	T
∆\$ kWh	=	\$27.14	T
∆\$ fuel oil	=	\$352.71	T

=

33

 $\Delta MMbtu_a$

<u>Walls</u> Wall SF Glaz SF Existing: 0* Insulation, R7 total New: 6* Insulation, R-5/in, R-38 total	6888 SF 240 SF 0.143 U 0.026 U	<u>Walls</u> ΔkWh _a =(((Wall Uvalue _{base} x Wall SF _{base})-(Wall Uvalue _{ee} x Wall SF _{ee}))x(T _{outdoor, design} - T _{indoor, setpoint})/ 1000)x EFLH _{cool} / IPLV ΔkWh _a =(((0.143 x 6888)-(0.026 x 6888))x(89 - 75)/ 1000)x 576 / 11.6 ΔkWh _a = 556
Cooling Efficiency (Existing wall a/c 9,000 btu, 11.2 EER max Cooling Efficiency, existing wall a/c 9,000 btu, 11.2 EER max Cooling Efficiency (Supplheat from plug-in and A/C, ase Heating Elec Efficiency (existing boiler) Use Heat COP to estimate slight heating pump power	, use avg) 9 EER 11.6 IPLV	
Use near COP to estimate slight heating pump power		ΔkWh _{heat} = 1330 No Electric Heat, but slight pumping power (converted btu and HP to COP)
		ΔkW _a =(((Wall Uvalue _{base} x Wall SF _{base})-(Wall Uvalue _{ee} x Wall SF _{ee}))x(T _{outdoor, design} - T _{indoor, setpoint})/ 1000)/ EER ΔkW _a =(((0.143 x 6888)-(0.026 x 6888))x(89 - 75)/ 1000)/ 9.0 ΔkW _a = 1.249
		$\Delta k W_{\rm cool} = 1.249$
		ΔkWa =(((Wall Uvalue _{base} x Wall SF _{base})-(Wall Uvalue _{se} x Wall SF _{ee}))x(T _{outdoor, design} - T _{indoor, setpoint})/ 1000)/ COPx3.412 ΔkWa =(((0.143 x 6888)-(0.026 x 6888))x(89 - 75)/ 1000)/ 68.2 ΔkWa = 0.165
		ΔkW _{heat} = 0.165 No Electric Heat, but slight pumping power (converted btu and HP to COP)
		ΔΜΜbtu _a =(((Wall Uvalue _{base} x Wall SF _{base})-(Wall Uvalue _{base} x Wall SF _{ee}))x(T _{indoor, setpoint} - T _{outdoor, design})/ 1000)x EFLH _{heat} / Eff _{FuelHeat} / 1000 ΔΜΜbtu _a =(((0.143 x 6888)-(0.026 x 6888))x(70 - 0)/ 1000)x 1616 / 80% / 1000 ΔΜΜbtu _a = 113
		ΔMMBtu = 113.472 Δfuel oil = 811
Air Inflitration Reduction -		Total ΔkWh = 1886 Total ΔkW = 1.413 $\Delta fuel oil$ = 811 $\Delta \$ kWh$ = \$314.09 $\Delta \$ fuel oil$ = \$1,202.86
air barrier, ceiling system - page 57	CF 0.69 ΔkWh/1000 ft ² 56	$ \Delta kWh = ft^{2}/1000 x(\Delta kWh/1000 ft^{2}) \Delta kWh = 5.4 x(56 \Delta kWh = 302.4 $
	$\begin{array}{ccc} \Delta kW/1000 \ ft^2 & 0.098 \\ ft^2 & 5400 \\ ft^2/1000 & 5.4 \\ \Delta therms/1000 \ ft^2 & 17 \end{array}$	$ \Delta kW = ft^2/1000 x (\Delta kW/1000 ft^2) x CF \Delta kW = 5.4 x (0.098 x 0.69 \Delta kW = 0.365148 $
		$ \Delta MMbtu = ft^{2}/1000 x (\Delta therms/1000 ft^{2}) / 10 \Delta MMbtu = 5.4 x (17) / 10 \Delta MMbtu = 9.18 \Delta fuel oil = 66 $
		Total ΔkWh = 302 Total ΔkW = 0.365 Δfuel oil = 66 Δ\$ kWh = \$50.36 Δ\$ fuel oil = \$97.31
		$TOTAL EEM-2$ $Total \Delta kWh = 2351$ $Total \Delta kW = 2.19$ $\Delta fuel oil = 1113.76$

∆fuel oil

∆\$kWh

∆\$ fuel oil

=

=

=

1113.76

\$391.59

\$1,652.88

EEM-3: HVAC Systems																				
EEM-3a : RTU with DX cooling																				
page 493																				
Code:DX Cooling, >=135 kbtuh <240 kbtu, 11.0 EER, 12.4 IEER	∆kWh _{RTU}	=	units	x(tons/unit	x(1	12/IEER _{base}	line -	12/IEER _{ee})x	EFLH _{Cool}	+	(kBTU/h)/unit	/ 3	.412 x(1/COP _{baselin}	.ne -	1/COPee)x	EFLH _{heat})
electric	∆kWh _{RTU}	=	1	X(12/1	×(12/9	-	12 / 12.2)x	575	+	300	/ 3	.412 x(1/2.5	-	1/1)x	1616)
	∆kWh _{RTU}	=	1	x(23	x(1.33		0.97)x	575	+	87.92		x(0.170	-	1.000)x	1616)
CF _{cooling} 0.8	ΔkWh _{RTU}	-	(113,143.72)		,				,					,				,	,
IEER _{ee} 12.4				-																
EER _{ee} 11	ΔkW _{RTU}	=	units	x(tons/unit	x(12/EER _{base}	ine -	12/EERee)x	CF _{cooling}									
(COP 1.0 w/ hot gas reheat) COP _{ee} 1	ΔkW _{RTU}	=	1	x(12/1	x(12/9		12/11)x	0.8									
EFLH _{heat} 1616	ΔkW _{RTU}	_	1	x	23	x(1.33		1.09)x	0.8									
	-	-		[^] ר	25	~(1.00		1.05)^	0.0									
EFLH _{Cool} 575	ΔkW _{RTU}	-	4.461																	
baseline steam boiler heating equipment capacity 800 MBH				-																
proposed heating load 300000 btuh	Δ\$ kWh	=	(\$18,843.10)																	
heat load 300 kBTU																				
proposed cooling load 23 tons	ΔMMBtu	=	units	x((kBTU/h _{heating}	/	unit)x(F _{fuelheat}	/	Eff _{heating,baselin}	_е)х(EFLH _{heating}	/ 1000))					
Eff _{heating,baseline} 80% Eff	ΔMMBtu	=	1	×((300	/	1)x(1	/	80%)x (1616	/ 1000))					
(Existing wall a/c 9,000 btu, 11.2EER max, use average) IEER _{baseline} 9	ΔMMBtu	=	606.000																	
(Supplemental heat from plug-in and A/C, assume 10%) COP baseline 2.5	∆fuel oil	=	4329																	
0.170 COP _{base}	∆\$ fuel oil	=	\$6,423.90																	
				-																
		EEM-3a																		

	EEM-3a	
Total ∆kWh	-	-113144
Total ∆kW	-	4.461
∆fuel oil	=	4328.597
∆\$ kWh	-	(\$18,843.10)
∆\$ fuel oil	=	\$6,423.90
	Total ΔkW Δfuel oil Δ\$ kWh	Total ΔkWh = Total ΔkW = Δfuel oil = Δ\$ kWh =

EEM-3b : High Efficient RTU with DX cooling

page 493																							
DX Cooling, >=135 kbtuh <240 kbtu, 12.0 EER, 13.7 IEER		∆kWh _{RTU}	=	units	x(tons/unit	x(12/IEER _{baselin}		12/IEERee)x	EFLH _{Cool}	+	(kBTU/h)/unit	/	3.41	2 x('	1/COP _{baseline}	e -	1/COPee)x	EFLH _{heat})	
		∆kWh _{RTU}	=	1	x(12/1	x(12 / 9	-	12/13.7)x	575	+	300	/	3.41	2 x(1/2.5	-	1/1)x	1616)	
		∆kWh _{RTU}	=	1	x(23	x(1.33		0.88)x	575	+	87.92			x(0.170		1.000)x	1616)	
CF _{cooling}	0.8	∆kWh _{RTU}	=	(111,929.28	в)																		
IEERee	13.7				4																		
EERee	12	ΔkW _{RTU}	-	units	x(tons/unit	×(12/EER _{baselin}		12/EER _{ee})x	CF _{cooling}											
(COP 1.0 w/ hot gas reheat) COPee	1	ΔkW _{RTU}	_	1	x(12/1	x(-	12 / 12.0		0.8											
EFLH _{heat}	1616	ΔkW _{RTU}	-	1	x(23	x(1.33	2	1.00)x)x	0.8											
						23	x(1.55	-	1.00)x	0.6											
EFLH _{Cool}	575	ΔkW _{RTU}	-	6.133	1																		
baseline steam boiler heating equipment capacity proposed heating load	800 MBH 300000 btuh	Δ\$ kWh	=	(\$18,640.84)	-																		
heat load	300 kBTU	∆ ∂ K wiii	-	(\$18,040.84)	_																		
proposed cooling load	23 tons	ΔMMBtu	=	units	x((kBTU/h _{heating}	/	unit)x(Ffuelheat	/ E	Fffhaating baselie) x (EFLHheating	/	1000))						
Effheating,baseline	80% Eff	ΔMMBtu	-	1	x((300	,	1)x(1	1	0.8)x (-	,	1000))						
(Existing wall a/c 9,000 btu, 11.2EER max, use average) IEERbaseline	9		-	606.000	п^((500	,)^(,	0.0)^(1010	,	1000	"						
(Supplemental heat from plug-in and A/C, assume 10%) COP _{baseline}					+																		
(Supplemental near from plug-in and A/G, assume 10%) COP baseline	2.5	Δfuel oil	-	4329 \$6.423.90	4																		
		Δ\$ fuel oil	=	\$6,423.90	1																		
Add VAV operation		∆kWh _{tan}	_	units	x	hp	x(∆kWh/hp)														
Motor hp	10 hp	∆kWh _{fan}	_	1	x	10	x(1606)														
(Appendix K, office, Poughkeepsie) ΔkWh/hp	1606	∆kWh _{fan}	-	16,060.00		10	~(1000	,														
(Appendix K, Olice, Poughkeepsie) ΔkW/hp	0.07	Liktentian	-	10,000.00																			
(Appendix R, Onice) ARWIND CF	0.8	∆kWh _{fan}	-	units	x	hp	x(∆kW/hp)x	CF													
qty	1 unit	∆kWh _{tan}	_	0.8	x	10	x()x	0.8													
qiy	1 unit	ΔkW _{fan}		0.448	пî	10	~(0.07)^	0.0													
	I	AR VV fan	-	0.440	-																		
		∆\$ kWh	=	\$2,674.65																			
Energy Recovery		-1		4 -,01 1100	-																		
Ventilation, 100% OA	2750 cfm OA	∆kWh _{ERU1}	=[((4.5	x	cfm OA	x(Eff _{hx, total}	-	Effhx, total base	e)x(Houtdoor, cooling	- a	Hindoor, cooling))/(1000	х	Eff _{ElecCool}))-	kW _{fan}]x	EFLH _{cool}	
	575 EFLH _{cool}	∆kWh _{ERU1}	=[((4.5	x	2750	x(-	0.00)x(28.80	-	25.30))/(1000	х	9.0))-	0.09]x	575	
	1616 EFLH _{heat}	∆kWh _{ERU1}	=	1609							, ,				<i>,,</i> , ,				.,				
	70 Tindoor, heating																						
	42.15 Toutdoor, heating	∆kWh _{cool}	-	1609	Т																		
	28.8 Houtdoor, cooling			1005	_																		
		A1-1A/I-		4.00		cfm OA		F #				-		-		1000		F #		-	,	1.147 1	
	25.3 Hindoor, cooling	∆kWh _{ERU1}	=[((1.08	x		x(Tindoor, heating		Toutdoor, heating		1000		Eff _{ElecHeat}))x	FElecHeat)-	kWfan]x	
		∆kWh _{ERU1}	=[((1.08	х	2750	x(0.60	-	0.00)x(70.00	-	42.15))/(1000	x	85.30))x	1)-	0.09]x	
0		∆kWh _{ERU1}	=	797																			
Cooling (When EER <= 14)	12.0 EER 14.44 SEER	∆kWh _{heat}	-	797	-																		
(When EER <= 14)	14.44 SEER 1 COP	Zakwy liheat	-	191	1																		
Additional fan power due to ER PD only	0.09 kW _{fan}	ΔkW_{ERU1}	=[((4.5	x	cfm OA	x(Eff _{hx, total}	-	Fff.)×(н		Hindoor, cooling	W/(1000	x	Eff _{ElecCool}))-	kW _{fan}]x	CF	
Additional fair power due to ETCPD only	0.6 Eff _{hx, total}	ΔkW _{ERU1}	=[((4.5	×	2750	x(-	0.00	e)x(Voutdoor, cooling 28.80	9 -	¹ indoor, cooling 25.30))/(1000	x	9.0))-	0.09]x	0.8	
	0.6 Eff _{hx, sens ee}	ΔkW _{ERU1}	=[((2.239	x	2750	x(0.60	-	0.00)X(20.00	-	25.30	<i>)</i> /(1000	x	9.0))-	0.09	lx	0.0	
	U.O Ellhx, sens ee	ΔKVV _{ERU1}	=	2.239																			
baseline - boiler 800MBH, 0.80ET	0.8	ΔkW	-	2.239	-																		
(Existing wall a/c 5,000 btu, 10.7 EER max) EERbaseline	9 EER	24.00	-	2.205	-																		
(Supplemental heat from plug-in and A/C, assume 10%) COP baseline	2.5 COP	Δ\$ kWh	=	\$400.69	Т																		
to approve the new new page and the two, assume to to baseline		±1¢ KVVII	-	\$400.03	4																		
	0 Eff _{hx, total base}							="				-		-				="		-			
	0 Eff _{hx, sens base}	∆MMbtu _{ERU1}	=[(1.08	х	cfm OA	×(Toutdoor, heating				Eff _{FuelHeat})]×	F _{FuelHeat}		EFLHheat	
		∆MMbtu _{ERU1}	=[(1.08	х	2750	x(0.60	-	0.00)x(70.00	-	42.15))/(1000000	х	0.80)]x	1	x	1616	
		∆MMbtu _{ERU1}	=	100.250																			
	i	ΔMMBtu	-	100.250	-																		
				716	+																		
		Δ\$ fuel oil	-	\$1,062.70	+																		
					-																		

	EEM-3b	
Total ∆kWh	-	-93463
Total ∆kW	=	8.820
∆fuel oil	-	5044.673
∆\$ kWh	=	(\$15,565.50)
∆\$ fuel oil	=	\$7,486,60

EFLH_{heat} 1616

EEM-3c: High Efficient Heat Pump					_																		
page 499					,		,				,												
		∆kWh _{RTU}	=	units	x(tons/unit		12/IEER _{baselin}		12/IEERee		EFLH _{Coo}		. ,		3.412		/COP _{baseline}		1/COP _{ee})x	EFLH _{heat})	
		ΔkWh _{RTU} ΔkWh _{RTU}	=	1	x(12 / 1 23	×(12/9	:	12 / 14.2	,	575 575	+	300	/	3.412	x(x(1 / 2.5 0.170	-	1/3.4)x	1616)	
CF _{cooling}	0.8		-		×(23	x(1.33	-	0.85)x	5/5	+	87.92			X(0.170	•	0.29)x	1616)	
UT cooling IEERee	14.2	ARVVIIRIU	-	(11,224.86)																		
	3.4	∆kW _{RTU}	-	units	x(tons/unit	~/	12/EER _{baselin}		12/EERee)x	CF _{cooling}											
EERee	13		-	1	x(x(12 / 1	×(×(12/EERbaselin 12/9	e -	12/EERee 12 / 14.2	,	0.8											
EFLH _{heat}	1616	ΔkW _{RTU}	-	1	x(23	×(1.33		0.92)x	0.8											
EFLH _{Cool}	575	ΔκΨητυ	-	7.549	¬^\	23	~(1.55	•	0.92)^	0.0											
	575	2.corkio	-	1.549																			
		Δ\$ kWh	-	(\$1,869.40)	7																		
baseline boiler heating equipment capacity	800 MBH				_																		
proposed heating load	300000 btuh	ΔMMBtu	=	units	×((kBTU/h _{heating}	/	unit)x(Ffuelheat		Eff _{heating,base}				1000))						
	300 kBTU	ΔMMBtu	=	1	×((300	/	1)x(1	/	80%)x (1616	/	1000))						
proposed cooling load	23 tons	ΔMMBtu	-	606.000	_																		
Effhesting,baseline	80% Eff	Δfuel oil	-	4329																			
(Existing wall a/c 5,000 btu, 10.7 EER max) IEER _{baseline}	9	∆\$ fue1 oil	=	\$6,423.90	_																		
(Supplemental heat from plug-in and A/C, assume 10%) COP _{baseline}	2.5	A1.34/h				h		A134/L /L	,														
Add VAV operation	75.6-	∆kWh _{fan} ∆kWh _{fan}	=	units	x	hp	×(∆kWh/hp)														
Motor hp (Appendix K, office, Poughkeepsie) ΔkWh/hp	7.5 hp 1606	ΔkWh _{fan}	-	1 12,045.00	٦×	7.5	×(1606)														
(Appendix K, omce, Pougnkeepsie) ΔkWn/np (Appendix K, Office) ΔkW/hp	0.07	AKW II fan	-	12,045.00																			
CF	0.8	∆kWh _{fan}	-	units	x	hp	x(∆kW/hp)x	CF													
qty	1 unit	∆kWh _{tan}	-	0.8	×	7.5	x(0.07)x	0.8													
**		ΔkW _{fan}	-	0.336	٦ .		(,														
		∆\$ kWh	-	\$2,005.99																			
		-+																					
Energy Recovery					_																		
Energy Recovery Ventilation, 100% OA	2750 cfm OA	∆kWh _{ERU1}	=[((4.5	×	cfm OA	x(Eff _{hx, total}		Eff _{hx, total bas}				indoor, cooling		1000		EffElecCool))-	kW _{fan}]x	EFLHcool	
	575 EFLH _{cool}	ΔkWh_{ERU1} ΔkWh_{ERU1}	=[((4.5	x x	cfm OA 2750	x(x(Eff _{hx, total} 0.60	-	Eff _{hx, total bas} 0.00	.e)x()x(H _{outdoor, coo} 28.80	ing -			1000 1000	x x	Eff _{ElecCool} 9.0))-))-	kW _{fan} 0.09]x]x	EFLH _{cool} 575	
	575 EFLH _{cool} 1616 EFLH _{heat}	∆kWh _{ERU1}																					
	575 EFLH _{cool} 1616 EFLH _{heat} 70 T _{indoor, heating}	ΔkWh _{ERU1} ΔkWh _{ERU1} ΔkWh _{ERU1}	=[((=	4.5 1609																			
	575 EFLH _{cool} 1616 EFLH _{heat} 70 T _{indoor, heating} 42.15 T _{outdoor, heating}	ΔkWh_{ERU1} ΔkWh_{ERU1}	=[((4.5																			
	575 EFLH _{cool} 1616 EFLH _{heat} 70 Tindoor, heating 42.15 Toutdoor, heating 28.8 Houtdoor, cooling	ΔkWh _{ERU1} ΔkWh _{ERU1} ΔkWh _{ERU1}	=[((= =	4.5 1609 1609	×	2750	x(0.60	-	0.00)x(28.80	-	25.30))/(1000	x	9.0))-	0.09]x	575	
	575 EFLH _{cool} 1616 EFLH _{heat} 70 T _{indoor, heating} 42.15 T _{outdoor, heating}	ΔkWh _{ERU1} ΔkWh _{ERU1} ΔkWh _{ERU1} ΔkWh _{cool}	=[((= = =[((4.5 1609 1609 1.08	× □ ×	2750 cfm OA	x(0.60 Eff _{hx, sens ee}	-	0.00 Eff _{hx, sens bas})x(.e)x(28.80 T _{indoor, heati}	- ng -	25.30 T _{outdoor, heating}))/(1000	x	9.0 Eff _{ElecHeat}))-))x	0.09 F _{ElecHeat}]×)-	575 kW _{fan}]x	
	575 EFLH _{cool} 1616 EFLH _{heat} 70 Tindoor, heating 42.15 Toutdoor, heating 28.8 Houtdoor, cooling	ΔkWh _{ERU1} ΔkWh _{ERU1} ΔkWh _{ERU1} ΔkWh _{cool} ΔkWh _{ERU1}	=[((= = =[((=[((4.5 1609 1609 1.08 1.08	×	2750	x(0.60 Eff _{hx, sens ee}	-	0.00)x(28.80	-	25.30 T _{outdoor, heating}))/(1000	x	9.0))-	0.09]x	575	
Ventilation, 100% OA	575 EFLH _{cool} 1616 EFLH _{heat} 70 Tindoor, heating 42.15 Toutdoor, heating 28.8 Hourdoor, cooling 25.3 H _{indoor} , cooling	ΔkWh _{ERU1} ΔkWh _{ERU1} ΔkWh _{ERU1} ΔkWh _{cool}	=[((= = =[((4.5 1609 1609 1.08	× □ ×	2750 cfm OA	x(0.60 Eff _{hx, sens ee}	-	0.00 Eff _{hx, sens bas})x(.e)x(28.80 T _{indoor, heati}	- ng -	25.30 T _{outdoor, heating}))/(1000	x	9.0 Eff _{ElecHeat}))-))x	0.09 F _{ElecHeat}]×)-	575 kW _{fan}]x	
Ventilation, 100% OA	575 EFLH _{cool} 1616 EFLH _{heat} 70 Tindoor, heating 42.15 Toutdoor, heating 28.8 Houtdoor, cooling	ΔkWh _{ERU1} ΔkWh _{ERU1} ΔkWh _{ERU1} ΔkWh _{cool} ΔkWh _{ERU1}	=[((= = =[((=[((4.5 1609 1609 1.08 1.08	× □ ×	2750 cfm OA	x(0.60 Eff _{hx, sens ee}	-	0.00 Eff _{hx, sens bas})x(.e)x(28.80 T _{indoor, heati}	- ng -	25.30 T _{outdoor, heating}))/(1000	x	9.0 Eff _{ElecHeat}))-))x	0.09 F _{ElecHeat}]×)-	575 kW _{fan}]x	
Ventilation, 100% OA	575 EFLH _{cool} 1616 EFLH _{heat} 70 Tindoor, heating 42.15 Toutdoor, heating 28.8 Hourdoor, cooling 25.3 Hindoor, cooling 13.0 EER	ΔkWh _{ERU1} ΔkWh _{ERU1} ΔkWh _{eRU1} ΔkWh _{eRU1} ΔkWh _{ERU1}	=[((= = =[((=	4.5 1609 1609 1.08 1.08 797	× □ ×	2750 cfm OA	x(0.60 Eff _{hx, sens ee}	-	0.00 Eff _{hx, sens bas})x(.e)x(28.80 T _{indoor, heati}	- ng -	25.30 T _{outdoor, heating}))/(1000	x	9.0 Eff _{ElecHeat}))-))x	0.09 F _{ElecHeat}]×)-	575 kW _{fan}]x	
Ventilation, 100% OA	575 EFLH _{col} 1616 EFLH _{heat} 70 T _{indsor} , heating 42.15 T _{outdoor} , heating 28.8 Houtdoor, cooling 25.3 H _{indsor} , cooling 13.0 EER 16.42 SEER	ΔkWh _{ERU1} ΔkWh _{ERU1} ΔkWh _{eRU1} ΔkWh _{eRU1} ΔkWh _{ERU1}	=[((= = =[((=	4.5 1609 1609 1.08 1.08 797	× □ ×	2750 cfm OA	x(0.60 Eff _{hx, sens ee}	-	0.00 Eff _{hx, sens bas})x(5e)x()x(28.80 T _{indoor, heati} 70.00	ng - -	25.30 T _{outdoor, heating} 42.15))/())/())/(1000	x x x	9.0 Eff _{ElecHeat}))-))x	0.09 F _{ElecHeat}]×)-	575 kW _{fan}]x	
Cooling (When EER <= 14)	575 EFLH _{cool} 1616 EFLH _{heat} 70 Tindoor, heating 42.15 Touckoor, heating 28.8 Houtdoor, cooling 25.3 H _{indoor} , cooling 13.0 EER 16.42 SEER 3.4 COP	AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1	=[((= = =[((= =	4.5 1609 1.08 1.08 797 797	× × ×	2750 cfm OA 2750	x(x(x(0.60 Eff _{hx, sens ee} 0.60	-	0.00 Eff _{hx, sens bas} 0.00)x(5e)x()x(28.80 T _{indoor, heati} 70.00	ng - -	25.30 Toutdoor, heating 42.15 H _{indoor, cooling}))/())/())/(1000 1000 1000	x x x	9.0 Eff _{ElecHeat} 85.30))-))x))x	0.09 F _{ElecHeat} 1]x)-)-	575 kW _{fan}]x 0.09]x	
Cooling (When EER <= 14)	575 EFLH _{cool} 1616 EFLH _{best} 70 Tindoor, heating 42.15 Toutdoor, heating 25.3 H _{indoor} , cooling 13.0 EER 16.42 SEER 3.4 COP 0.09 kWr _{1an}	AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1	=[((= = = = [((4.5 1609 1.08 1.08 1.08 797 797 4.5		2750 cfm OA 2750 cfm OA	x(x(x(x(0.60 Eff _{hx, sens ee} 0.60 Eff _{hx, total}	-	0.00 Eff _{hx, sens bas} 0.00 Eff _{hx, total bas})x(se)x()x(se)x(28.80 T _{indoor, heati} 70.00	- ng - -	25.30 Toutdoor, heating 42.15 H _{indoor, cooling}))/())/())/(1000 1000 1000	x x x	9.0 Eff _{ElecHeat} 85.30))-))x))x	0.09 F _{ElecHeat} 1 kW _{fan}]x)-)-	575 kW _{fan}]x 0.09]x CF	
Cooling (When EER <= 14) Additional fan power due to ER PD only	575 EFLH _{cool} 1616 EFLH _{best} 70 Tindoor, heating 42.15 Toudoor, heating 28.8 Houdsor, cooling 25.3 Hindoor, cooling 13.0 EER 16.42 SEER 3.4 COP 0.09 kWran 0.6 Efflex, total 0.6 Efflex, sense ee	AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWeru1 AkWeru1 AkWeru1	=[((= = = = [((= = [((=	4.5 1609 1.08 1.08 797 797 4.5 4.5 4.5 2.239		2750 cfm OA 2750 cfm OA	x(x(x(x(0.60 Eff _{hx, sens ee} 0.60 Eff _{hx, total}	-	0.00 Eff _{hx, sens bas} 0.00 Eff _{hx, total bas})x(se)x()x(se)x(28.80 T _{indoor, heati} 70.00	- ng - -	25.30 Toutdoor, heating 42.15 H _{indoor, cooling}))/())/())/(1000 1000 1000	x x x	9.0 Eff _{ElecHeat} 85.30))-))x))x	0.09 F _{ElecHeat} 1 kW _{fan}]x)-)-	575 kW _{fan}]x 0.09]x CF	
Cooling (When EER <= 14) Additional fan power due to ER PD only baseline - boiler 800MBH , 0.80ET	575 EFLH _{cool} 1616 EFLH _{bast} 70 Tindoor, heating 28.8 Houtdoor, cooling 25.3 Hieddoor, cooling 13.0 EER 16.42 SEER 3.4 COP 0.09 kWYran 0.6 Effhu, total 0.6 Effhus, sens ee 0.8	AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWeru1	=[((= =[((= =[((=[((4.5 1609 1.08 1.08 797 797 4.5 4.5		2750 cfm OA 2750 cfm OA	x(x(x(x(0.60 Eff _{hx, sens ee} 0.60 Eff _{hx, total}	-	0.00 Eff _{hx, sens bas} 0.00 Eff _{hx, total bas})x(se)x()x(se)x(28.80 T _{indoor, heati} 70.00	- ng - -	25.30 Toutdoor, heating 42.15 H _{indoor, cooling}))/())/())/(1000 1000 1000	x x x	9.0 Eff _{ElecHeat} 85.30))-))x))x	0.09 F _{ElecHeat} 1 kW _{fan}]x)-)-	575 kW _{fan}]x 0.09]x CF	
Cooling (When EER <= 14) Additional fan power due to ER PD only baseline - boiler 800MBH , 0.80ET (Existing wall a/c 5,000 btu, 10.7 EER max) EERstassine	575 EFLH _{cool} 1616 EFLH _{bast} 70 Tindoor, heating 28.8 Houtdoor, cooling 25.3 Hindoor, cooling 13.0 EER 16.42 SEER 3.4 COP 0.09 kW(ran 0.6 Effhar, sens ee 0.8 9 EER	AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1	=[((= = = = = = = = = = = = = = = = =	4.5 1609 1.08 1.08 797 797 4.5 4.5 2.239 2.239		2750 cfm OA 2750 cfm OA 2750	x(x(x(x(0.60 Eff _{hx, sens ee} 0.60 Eff _{hx, total} 0.60	-	0.00 Eff _{hx, sens bas} 0.00 Eff _{hx, total bas} 0.00)x(se)x()x(se)x()x(28.80 T _{indoor, heat} 70.00 H _{outdoor, coo} 28.80	- - ing - -	25.30 T _{outdoor, heating} 42.15 H _{indoor, cooling} 25.30))/())/())/(1000 1000 1000 1000	x x x x	9.0 Eff _{ElecHeat} 85.30 Eff _{ElecCool} 9.0))-))x))x))-))-	0.09 F _{ElecHeat} 1 kW _{fan} 0.09)+)-)-]x]x	575 kW _{fan} x 0.09 x CF 0.8	
Cooling (When EER <= 14) Additional fan power due to ER PD only baseline - boiler 800MBH , 0.80ET	575 EFLH _{cool} 1616 EFLH _{beat} 70 Tindoor, heating 24.15 Toutdoor, heating 28.8 Houndoor, cooling 25.3 H _{indoor} , cooling 13.0 EER 16.42 SEER 3.4 COP 0.09 kWr ₄ n 0.6 Eff _{bx} , sena ee 0.8 9 EER 2.5 COP	AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1	=[((= = = = = = = = = = = = = = = = = [(4.5 1609 1.08 1.08 797 797 4.5 4.5 2.239 2.239 1.08		cfm OA 2750 cfm OA 2750 cfm OA	x(x(x(x(x(x(0.60 Eff _{hx, sens ee} 0.60 Eff _{hx, total} 0.60	-	0.00 Eff _{hx, sens bas} 0.00 Eff _{hx, total bas} 0.00 Eff _{hx, sens bas})x(28.80 T _{indoor, heati} 70.00 H _{outdoor, coo} 28.80 T _{indoor, heati}	- - ing - -	25.30 Toutdoor, heating 42.15 Hendoor, cooling 25.30))/())/())/())/())/(1000 1000 1000 1000 1000	x x x x x	9.0 Eff _{ElecHeat} 85.30 Eff _{ElecCool} 9.0))-))x))x))-))-	0.09 F _{ElecHeat} 1 kW _{fan} 0.09)-)-)-]x]x]x	575 kW _{fan}]x 0.09]x CF 0.8 EFLH _{heat}	
Cooling (When EER <= 14) Additional fan power due to ER PD only baseline - boiler 800MBH , 0.80ET (Existing wall a/c 5,000 btu, 10.7 EER max) EERstassine	575 EFLH _{cool} 1616 EFLH _{best} 70 Tindoor, heating 42.15 Toutdoor, heating 25.3 H _{indoor} , cooling 25.3 H _{indoor} , cooling 13.0 EER 16.42 SEER 3.4 COP 0.09 kWr _{1an} 0.6 Eff _{hx, total} 0.6 Eff _{hx, total} 0.8 9 EER 2.5 COP 0 Eff _{hx, total} hase	AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1	=[((= = = = = = = = = = = = = = = = = [(= = = =	4.5 1609 1.08 1.08 797 797 4.5 4.5 2.239 2.239 1.08 1.08		2750 cfm OA 2750 cfm OA 2750	x(x(x(x(0.60 Eff _{hx, sens ee} 0.60 Eff _{hx, total} 0.60	-	0.00 Eff _{hx, sens bas} 0.00 Eff _{hx, total bas} 0.00)x(se)x()x(se)x()x(28.80 T _{indoor, heat} 70.00 H _{outdoor, coo} 28.80	- - ing - -	25.30 Toutdoor, heating 42.15 Hendoor, cooling 25.30))/())/())/())/())/(1000 1000 1000 1000	x x x x	9.0 Eff _{ElecHeat} 85.30 Eff _{ElecCool} 9.0))-))x))x))-))-	0.09 F _{ElecHeat} 1 kW _{fan} 0.09)+)-)-]x]x	575 kW _{fan} x 0.09 x CF 0.8	
Cooling (When EER <= 14) Additional fan power due to ER PD only baseline - boiler 800MBH , 0.80ET (Existing wall a/c 5,000 btu, 10.7 EER max) EERstassine	575 EFLH _{cool} 1616 EFLH _{beat} 70 Tindoor, heating 24.15 Toutdoor, heating 28.8 Houndoor, cooling 25.3 H _{indoor} , cooling 13.0 EER 16.42 SEER 3.4 COP 0.09 kWr ₄ n 0.6 Eff _{bx} , sena ee 0.8 9 EER 2.5 COP	AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1	=[((= = = = = = = = = = = = = = = = = [(4.5 1609 1.08 1.08 797 797 4.5 4.5 2.239 2.239 1.08		cfm OA 2750 cfm OA 2750 cfm OA	x(x(x(x(x(x(0.60 Eff _{hx, sens ee} 0.60 Eff _{hx, total} 0.60	-	0.00 Eff _{hx, sens bas} 0.00 Eff _{hx, total bas} 0.00 Eff _{hx, sens bas})x(28.80 T _{indoor, heati} 70.00 H _{outdoor, coo} 28.80 T _{indoor, heati}	- - ing - -	25.30 Toutdoor, heating 42.15 Hendoor, cooling 25.30))/())/())/())/())/(1000 1000 1000 1000 1000	x x x x x	9.0 Eff _{ElecHeat} 85.30 Eff _{ElecCool} 9.0))-))x))x))-))-	0.09 F _{ElecHeat} 1 kW _{fan} 0.09)-)-)-]x]x]x	575 kW _{fan}]x 0.09]x CF 0.8 EFLH _{heat}	
Cooling (When EER <= 14) Additional fan power due to ER PD only baseline - boiler 800MBH , 0.80ET (Existing wall a/c 5,000 btu, 10.7 EER max) EERstassine	575 EFLH _{cool} 1616 EFLH _{best} 70 Tindoor, heating 42.15 Toutdoor, heating 25.3 H _{indoor} , cooling 25.3 H _{indoor} , cooling 13.0 EER 16.42 SEER 3.4 COP 0.09 kWr _{1an} 0.6 Eff _{hx, total} 0.6 Eff _{hx, total} 0.8 9 EER 2.5 COP 0 Eff _{hx, total} hase	AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1	=[((= = = = = = = = = = = = = = = = = [(= = = =	4.5 1609 1.08 1.08 797 797 4.5 4.5 2.239 2.239 1.08 1.08		cfm OA 2750 cfm OA 2750 cfm OA	x(x(x(x(x(x(0.60 Eff _{hx, sens ee} 0.60 Eff _{hx, total} 0.60	-	0.00 Eff _{hx, sens bas} 0.00 Eff _{hx, total bas} 0.00 Eff _{hx, sens bas})x(28.80 T _{indoor, heati} 70.00 H _{outdoor, coo} 28.80 T _{indoor, heati}	- - ing - -	25.30 Toutdoor, heating 42.15 Hendoor, cooling 25.30))/())/())/())/())/(1000 1000 1000 1000 1000	x x x x x	9.0 Eff _{ElecHeat} 85.30 Eff _{ElecCool} 9.0))-))x))x))-))-	0.09 F _{ElecHeat} 1 kW _{fan} 0.09)-)-)-]x]x]x	575 kW _{fan}]x 0.09]x CF 0.8 EFLH _{heat}	
Cooling (When EER <= 14) Additional fan power due to ER PD only baseline - boiler 800MBH , 0.80ET (Existing wall a/c 5,000 btu, 10.7 EER max) EERstassine	575 EFLH _{cool} 1616 EFLH _{best} 70 Tindoor, heating 42.15 Toutdoor, heating 25.3 H _{indoor} , cooling 25.3 H _{indoor} , cooling 13.0 EER 16.42 SEER 3.4 COP 0.09 kWr _{1an} 0.6 Eff _{hx, total} 0.6 Eff _{hx, total} 0.8 9 EER 2.5 COP 0 Eff _{hx, total} hase	AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkW	=[((= = = = = = = = = = = = = = = = = =	4.5 1609 1.08 1.08 797 4.5 4.5 2.239 2.239 1.08 1.08 1.08 100.250		cfm OA 2750 cfm OA 2750 cfm OA	x(x(x(x(x(x(0.60 Eff _{hx, sens ee} 0.60 Eff _{hx, total} 0.60	-	0.00 Eff _{hx, sens bas} 0.00 Eff _{hx, total bas} 0.00 Eff _{hx, sens bas})x(28.80 T _{indoor, heati} 70.00 H _{outdoor, coo} 28.80 T _{indoor, heati}	- - ing - -	25.30 Toutdoor, heating 42.15 Hendoor, cooling 25.30))/())/())/())/())/(1000 1000 1000 1000 1000	x x x x x	9.0 Eff _{ElecHeat} 85.30 Eff _{ElecCool} 9.0))-))x))x))-))-	0.09 F _{ElecHeat} 1 kW _{fan} 0.09)-)-)-]x]x]x	575 kW _{fan}]x 0.09]x CF 0.8 EFLH _{heat}	
Cooling (When EER <= 14) Additional fan power due to ER PD only baseline - boiler 800MBH , 0.80ET (Existing wall a/c 5,000 btu, 10.7 EER max) EERbaseline	575 EFLH _{cool} 1616 EFLH _{best} 70 Tindoor, heating 42.15 Toutdoor, heating 25.3 H _{indoor} , cooling 25.3 H _{indoor} , cooling 13.0 EER 16.42 SEER 3.4 COP 0.09 kWr _{1an} 0.6 Eff _{hx, total} 0.6 Eff _{hx, total} 0.8 9 EER 2.5 COP 0 Eff _{hx, total} hase	AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWheru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkWeru1 AkW	=[((= = = = = = = = = = = = = = = = = =	4.5 1609 1.08 1.08 797 797 4.5 4.5 2.239 2.239 1.08 1.08 1.08 100.250		cfm OA 2750 cfm OA 2750 cfm OA	x(x(x(x(x(x(0.60 Eff _{hx, sens ee} 0.60 Eff _{hx, total} 0.60	-	0.00 Eff _{hx, sens bas} 0.00 Eff _{hx, total bas} 0.00 Eff _{hx, sens bas})x(28.80 T _{indoor, heati} 70.00 H _{outdoor, coo} 28.80 T _{indoor, heati}	- - ing - -	25.30 Toutdoor, heating 42.15 Hendoor, cooling 25.30))/())/())/())/())/(1000 1000 1000 1000 1000	x x x x x	9.0 Eff _{ElecHeat} 85.30 Eff _{ElecCool} 9.0))-))x))x))-))-	0.09 F _{ElecHeat} 1 kW _{fan} 0.09)-)-)-]x]x]x	575 kW _{fan}]x 0.09]x CF 0.8 EFLH _{heat}	

	EEM-3c	
Total ∆kWh	=	3226
Total AkW	=	10.124
∆fuel oil	=	5044.673
Δ\$ kWh	=	\$537.28
∆\$ fuel oil	=	\$7,486.60

M/E Reference 211222

EFLH_{heat} 1616

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EEM-3d: VRF System (pg 151/168) page 168 EFLH _{boating} 575 EFLH _{boating} 1616 cool tons 23	ΔkWh ΔkWh ΔkWh ΔkWh	= = =	units 1 1 (9,384.1	x((x((kBTU/h _{cooling} 276 276	g / / /	unit 1 1	x(x(x(1	 	EER _{baseline} 9 9		1 / 17)x)x)x	EFLH _{cooling} 575 575	+(k +(+(BTU/h _{heating} 300 87.92	X 3.412 41200	× × ×	F _{elecheat} 1 0.170	1	COP _{baseline} 2.5	-	0.233 1/COP _{ee} 1 / 3.4 0.294)x)x)x	EFLH _{heating} 1616 1616
kBTU/hooding 276 kBTU/hooding 300 Face 1 EERee 17 COPee 3.4	ΔkW ΔkW ΔkW	=	units 1 9.958	×[(×[(kBTU/h _{cooling} 276	, / /	unit 1)x(()x((1	1682.345 0.061 EER _{baseline} 9) - () - ())x))x	CF 0.69	1										
CF 0.69 F _{Fusheat} 1 Eff _{basting baseline} 0.8 F _{electeat} 1	ΔMMBtu ΔMMBtu ΔMMBtu Δfuel oil	= = =	units 1 606.000 4329	×((×((kBTU/h _{heatin} 300	g / /	unit 1)x()x(F _{fuelheat} 1	1	Eff _{heating,baseli} 0.8	ne)x ()x (, /))))										
baseline - boiler 800MBH , 0.80ET (Existing wall a/c 9,000 btu, 11.2 EER max) EER _{pasteline} 9 (Supplemental heat from plug in and A/C, assume 10%) COP _{basteline} 2.5																										
Add VAV operation Motor hp 7.5 hp (Appendix K, office, Poughkeepsie) ΔkWh/hp 1606 (Appendix K, Office) ΔkWh/hp 0.07 CF 0.8 qty 1 unit	ΔkWh _{fan} ΔkWh _{fan} ΔkWh _{fan} ΔkWh _{fan} ΔkW _{fan} ΔkW _{fan}		units 1 12,045.0 units 0.8 0.336 \$2,005.99		hp 7.500 hp 7.500	x(x(x(x(1606)																		
Energy Recovery Ventilation, 100% OA 2750 cfm O/ EFLH _{cosing} 575 EFL EFLH _{beating} 1616 EFL 1010 2710 Track 42.15 Toutoon 42.15	H _{cool} ΔkWh _{ERU1} heat ΔkWh _{ERU1} heating ΔkWh _{cool}	=[((=[((=	4.5 4.5 1609 1609	×××	cfm OA 2750	x(x(H _{outdoor, coolin} 28.80		H _{indoor, coolin} 25.30					W _{fan}]x).09]x		EFLH _{cool} 575						
28.8 H _{outdoo} 25.3 H _{indoor} Cooling 13.0 EER	coling ΔkWh _{ERU1} ΔkWh _{ERU1} ΔkWh _{ERU1}	=	1.08 1.08 797	x x	cfm OA 2750	x(x(Eff _{hx, sens ba} 0.00		T _{indoor, heating} 70.00		T _{outdoor, heatin} 42.15			x x		lecHeat)- 1)-		kW _{fan}]) 0.09])		EFLH _{heat} 1616				
(When EER <= 14) 16.42 SEER 3.4 COP Additional fan power due to ER PD only 0.09 kW 0.6 Eff _{tex, to} 0.6 Eff _{tex} ,	ΔkW _{ERU1}	= =[((=[((=	4.5 4.5 2.239	x x	cfm OA 2750	x(x(H _{outdoor, coolin} 28.80	g - -				x x		W _{fan}]x).09]x		CF 0.8						
baseline - steam boller 600MBH , 0.80ET 0.8 (Existing wall a/c 9,000 btu, 11.2 EER max) EERbaseline 9 EER (Supplemental heat from plug in and A/G, assume 10%) COPPusative 2.5 COP 0 Effe 0 Effe		=[(2.239 1.08 1.08 100.250 100.250		cfm OA 2750						Tindoor, heating 70.00							uelHeat X 1 X		EFLH _{heat} 1616						
	Δinibut Δfuel oil Total ΔkWh Total ΔkW Δfuel oil Δ\$ kWh Δ\$ fuel oil	= EEM-3d	716 5067 12.533 5044.673 \$843.84 \$7,486.60																							

EEM-3e: GSHP (pg 562) EFLH _{heating} COPseason, ee - Closed loop COP season,base	1616 3.6 2.500	ΔkWh ΔkWh ΔkWh ΔkWh	=[=[=[BCL/1000 235208/1000 276 -8307	×(×(×(1/9	- 1/ - -	/EER _{season,ee} 1/15 0.067)x)x)x	EFLH _{cooling} 575 575		BHL/3,412 326521/3,412 87.925		F _{elecheat} 0	/ 0 / 0.170	OP _{season,b} 2.500	_{ase} - 1 - -	/COP _{season,} 1/3 0.278	ee)x)x)x	EFLH _{heating} 1616 1616	9			
Felecheat BHL - heating load (BTU/h) 3 BCL - cooling load (BTU/h) 2 EFLHcooling EERseason,ee - closed loop	76000 575 15	ΔkW ΔkW ΔkW ΔkW	= = =	235208/1000		1/EER _{peak,season} - 1/11.2 - 0.089 -	1/1)x ().8														
EERseason,base , EERpeak,season EERGSHP,kuit,ee CF, Coincidence Factor Frustreat	9 11.2 18.1 0.8 1	ΔMMBtu ΔMMBtu ΔMMBtu ΔMMBtu	=	BHL/1,000,000 326521/1,000,000 0.3 606.000	××××	F _{fueiHeat} 1 1	/ / /	Eff _{baseline} 0.8 0.8	x x x	EFLH _{heating} 1616 1616														
Eff _{baseline} baseline - boiler 800MBH , 0.80ET	0.8	Δfuel oil	-	4329]																			
Add VAV operation Motor hp (Appendix K, office, Poughkeepsie) ΔkW/hi (Appendix K, Office) AkW/h	7.5 hp 1606 [∆kWh _{fan} ∆kWh _{fan} ∆kWh_{fan}	-	units 1 12,045.00	××		x(x())															
CF qty	0.8 1 unit	ΔkWh _{fan} ΔkWh _{fan} ΔkW_{fan}	-	units 0.8 0.336	××		x(x(∆kW/hp 0.07)x)x	CF 0.8														
Energy Recovery	Ļ	Δ\$ kWh	=	\$2,005.99																				
Ventilation, 100% OA EFLH _{cooling} EFLH _{heating}	2750 cfm OA 575 EFLH _{cool} 1616 EFLH _{heat} 70 T _{indoor, heating}	ΔkWh _{ERU1} ΔkWh _{ERU1} ΔkWh _{ERU1}	=[((=[((=	4.5 4.5 1609	x x		x(x(- 1	Eff _{hx, total base} 0.00)x()x(Houtdoor, cooling 28.80	-	H _{indoor, cooli} 25.30	ng))/())/(1000 1000	x x	Eff _{ElecCool} 9.0))-))-	kW _{fan} 0.09]x]x	EFLH _{co} 575	ы	
	42.15 Toutdoor, heating 28.8 Houtdoor, cooling 25.3 Hindoor, cooling	ΔkWh _{cool} ΔkWh _{ERU1} ΔkWh _{ERU1} ΔkWh _{ERU1}	= =[((=[((=	1609 1.08 1.08 797	× ×		x(I x(Eff _{hx, sens ee} 0.60	- E -	Eff _{hx, sens base} 0.00)x()x(-			1000 1000	x x	Eff _{ElecHeat} 85.30))x))x	F _{ElecHeat})-)-	kW _{fan} 0.09		EFLH _{heat} 1616
Cooling (When EER > 14)	17.0 EER 19.43 SEER	ΔkWh _{heat}	-	797]																			
Additional fan power due to ER PD only	4.3 COP 0.09 kW _{fan} 0.6 Eff _{hx, total} 0.6 Eff _{hx, sens ee}	ΔkW _{ERU1} ΔkW _{ERU1} ΔkW _{ERU1}	=[((=[((=	4.5 4.5 2.239	x x		x(x(- 1	Eff _{hx, total base} 0.00)x()x(H _{outdoor, cooling} 28.80	-		ng))/())/(1000 1000	x x	Eff _{ElecCool} 9.0))-))-	kW _{fan} 0.09]x]x	CF 0.8		
baseline - boiler 800MBH , 0.80ET (Existing wall a/c 9,000 btu, 11.2 EER max) EER _{baseline} (Supplemental heat from plug-in and A/C, assume 10%) COP _{baseline}	0.8 9 EER 2.5 COP 0 Eff _{hx, total base} 0 Eff _{hx, sens base}	ΔkW ΔMMbtu _{ERU1} ΔMMbtu _{ERU1} ΔMMbtu _{ERU1}	= =[(=[(=	2.239 1.08 1.08 100.250] × ×		x(I x(Eff _{hx, sens ee} 0.60	- 6	Eff _{hx, sens base} 0.00)x()x(T _{indoor, heating} 70.00	-			1000000 1000000		Eff _{FuelHeat} 0.80)]×)]x	F _{FuelHeat} 1		EFLH _{hea} 1616		
	Ē	ΔMMBtu Δfuel oil	= = EEM-3e	100.250 716]																			

	EEM-3e	
Total ∆kWh	=	6144
Total AkW	-	10.090
∆fuel oil	=	5044.673
∆\$ kWh	=	\$1,023.20
∆\$ fuel oil	=	\$7,486.60

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EEM-4: Domestic Hot Water	
Occupied days per year 365 Da	
UEF baseline 0.8400 UE PoughkeepisiF _{man} 558 PF PoughkeepisiF _{man} 588 PF Test 408 PF Test 140 GPD from p44b table 110 Etm., AFUEm, assumed eff of fossil kel hig sys 92%	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$
Et _{base} , AFUE , assumed eff of fossil fuel htg sys 80%	Δ <i>kW</i> = 0.170
ASHP SEER 13 ASHP HSPF 8.2 Funces 1 UEF _{Rec} Progone and Electric 0.92 UE UEF _{Rec} ASHP 2.5 UE UEF _{Rec} ASHP 3 UE	F <u>Δhuel oil = 120</u>
Factors 1.00 Front 0.51 FLCO 1 Factors 1 Factors 0.43 Front 0.05 Front 0 PolotOPHY 1 FFEDHW 1.0 Electric SEER 3.412 GSHP HSPF 3.512 GSHP HSPF 5.5	ΔΔMMBu = units x(GPD x 365 x 3.33 x Δ1mm y 100000 x(Pacewark 4.464076 Yebseline H PloaderHMV/ AFULE X 10 x 365 x 8.33 x 144955.8 y 100000 x(PloaderHMV 25% x(10.480 H 0/ 80%, H 0/2 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 0.6125 ΔMMBbu = -1681 - - - 1 x 1 x 0.6125 x - 1.87 <t< td=""></t<>
	EEM_th: DHW sensed by Electric Loht ΔΔWh = units x(QPO x 365 x 8.33 x ΔT _{main})/ 3412 x(F _{aCHV} / UEF _{baselina} -(1/ UEF _{ma} x F _{abrea}))+ ΔΔWh _{basting} - ΔΔWh _{basting} ΔΔWh = 1 x(88.537 x 365 x 8.33 x 140-56.8)/ 3412 x(0 / 0.8400 -(1/ 0.92 x 1.00))+ 442 - 674 ΔΔWh = 1 x(88.537 x 365 x 8.33 x 84.2)/ 3412 x(0.00 -(1.087))+ 442 - 674 <u>ΔWh = 1 x</u> (2266587/334)/ 3412 x(0.007 -(1.087))+ 442 - 674
	ΔXVM heading = units x(GPD x 365 x 8.33 x ΔTmain y 3412 x(1/UEFan)x FLOC x(FLOC x(FLOC x(50.517)x ΔKVM heading = 1 x(88.537 x 365 x 8.33 x 140-55.8 y 3412 x(1/.92)x 1 x(0.51/2) ΔKVM heading = 1 x(88.537 x 86.33 x 64.2 y 3412 x(1.087)x 1 x(0.510) ΔKVM heading = 1 x(22865887.334 y 3412 x(1.087)x 1 x(0.510) ΔKVM heading = 3683 3412 x(1.087)x 1 x(0.510)
	AWMPmanng = units x/ GPD x 365 x 8.13 x ATmain y 3412 x/ 1/UEFmg jx Froz x Fmain K Fmain HSPF12412 AWMPmanng = 1 x/ 88.537 x 363 x A422 y/ 3412 x(1/02 x 4.99/12/1412 AWMPmanng = 1 x/ 88.537 x 363 x 84.22 y/ 3412 x(1/087 jx 1 x 1/04 AWMPmanng = 1 x/ 2666587.33 x 8.42 y/ 3412 x(1/087 jx 1 x 1/04 AWMPhantrag = 1 x/ 2666587.33 y/ 3412 x(1/087 jx 1 x 0.497 AWMPhantrag = 3536 x//// 1/087 jx 1 x 1 x 0.497
	ΔKW = units x(ΔKW / unit) ΔKW = 1 x 0.211 ΔKW = 0.211 ΔMMBiu = units x(GPD x 365 x 8.33 x ΔT _{max} V 100000 x/(FFFDHW / UEPbaseline Hr (FbolledDHW / AFUE H 1/1/IFFen x Floc x FlueIheat x Fheat/AFUE)
	ΔΜΜΒ ₁₀ = 1 x{ 21.463 x 365 x 8.33 x 149-55.8 y 1000000 x{(1.0 / 0.8400)+{ 1/ 0.95 } { 0.52 } x 1 x 0 x 0.4980%) ΔΜΜΒ ₁₀ = 1 x{ ΔΜΜΒ ₁₀ = 1 x{ ΔΜΜΒ ₁₀ = 1 x{ ΔΜΜΒ ₁₀ = 1 x{ ΔΜΜΒ ₁₀ = 1 x 0 x 0.6125) Δημείου = 96 Δημείου = 96 ΕΕΜ-Δ
	Total ΔWW = 224 Total ΔWW = 0.041 Δfuel oil = 119.731 Δ\$ \$kwh = \$37.77 Δ\$ \$kuel oil = \$177.69

EEM-4c: DHW se	erved by Ai	r Source Heat Pu	ump_																									
ΔkWh ΔkWh ΔkWh ΔkWh	= = =	units 1 1 5019	x(x(x(x(GPD 110.000 88.537 22665887.334	x x x	365 365 365	x x x	8.33 8.33 8.33	x x x	ΔT _{main} 140-55.8 84.2	y y y y	3412 3412 3412 3412	x(x(x(x(F _{eDHW} 1 1.190 0.790	/ /	UEF _{baseline} 0.8400	-(1/ -(1/ -(0.400	UEF _{ee}	x 2.5 x	F _{derae}))+ 1.00))+))+))+		∆kWh _{cooling} 442 442 442	-	ΔkWh _{heating} 674 674 674			
ΔkWh _{cooling} ΔkWh _{cooling} ΔkWh _{cooling} ΔkWh _{cooling} ΔkWh _{cooling}	= = = =	units 1 1 1 442	x(x(x(x(x x x	365 365 365	x x x	8.33 8.33 8.33	x x x	ΔT _{main} 140-55.8 84.2	y y y y	3412 3412 3412 3412	x(x(x(x(1/UEFee 1/2.5 0.400 0.400)x)x)x)x	FLOC 1 1 1	x(F _{cool} / x(0.51/ x(0.134 x(0.134	13/3.4	3.412) 12))									
ΔkWh _{heating} ΔkWh _{heating} ΔkWh _{heating} ΔkWh _{heating}	= = = =	units 1 1 674	×(×(×(×(GPD 110.000 110.000	x x x		x x x 60647.900	8.33 8.33 8.33	x x x	ΔT _{main} 140-55.8 84.2	y y y y	3412 3412 3412 3412	x(x(x(x(1/UEF _{ee} 1/2.5 0.400 0.400)x)x)x)x	FLOC 1 1 1	x F _{elechez} x 1 x 1 x 1 x 1	at))))	0.49 0.49	/ 8.2/3	3.412							
ΔkW ΔkW ΔkW ΔMMBtu ΔMMBtu	=	units 1 0.061 units 1	×(× ×(×(ΔkW 0.061 GPD 21.463	/ x x	unit) 365 365	x x	8.33 8.33	x x	ΔT _{main} 140-55.8	y y	1000000	x((FFFDHW 1.0	/	0.8400)+(FboilerDH)+(1/	80	%)-(1/UEF 1/2.5		x x	Floc 1	x x	Ffuelheat 0	x x	Fheat/AFUE 0.49/80%)
ΔMMBtu ΔMMBtu Δfuel oil Total ΔkWh Total ΔkW Δfuel oil Δ\$ kWh	= = = EEM-4c = = = =	1 13.410 96 5019 0.061 119.731 \$835.90 \$177.69	×(549	94760.566				У	1000000	×((1.0	/	0.8400)+(1.25	ж		0.400	x	1	x	0	x	0.6125)
EEM-4d: DHW ser ΔkWh ΔkWh ΔkWh ΔkWh ΔkWh	nved by geo = = = = =		± ×(×(×(GPD 88.537 88.537 22665887.334	x x x	365 365 365	x x x	8.33 8.33 8.33	x x x	ΔT _{main} 140 -55.8 84.2	y y y	3412 3412 3412 3412	x(x(x(x(F _{eDHW} 1 1.190 0.857	/	UEF _{baseline} 0.8400	-(1/ -(1/ -(0.333	UEF _{ee}	x 3 x	F _{derae}))+ 1.00))+))+))+		∆kWh _{cooling} 296 296 296	-	∆kWh _{heating} 387 387 387			
ΔkWh _{cooling} ΔkWh _{cooling} ΔkWh _{cooling} ΔkWh _{cooling}	= = = =	units 1 1 296	x(x(x(x(GPD 88.537 88.537 22665887.334	x x x	365 365 365	x x x	8.33 8.33 8.33	x x x	ΔT _{main} 140 -55.8 84.2	y y y	3412 3412 3412 3412	x(x(x(x(1/UEF _{ee} 1/3.0 0.333 0.333)x)x)x)x	FLOC 1 1	x(F _{cool} / x(0.51/ x(0.134 x(0.134	13/3.4	3.412) 12))									
ΔkWh _{heating} ΔkWh _{heating} ΔkWh _{heating} ΔkWh _{heating} ΔkWh _{heating}	= = = =	units 1 1 1 387	x(x(x(x(GPD 88.537 88.537	x x x	365 365 365 226	x x x 65887.334	8.33 8.33 8.33	x x x	ΔT _{main} 140 -55.8 84.2	y y y y	3412 3412 3412 3412	x(x(x(x(1/UEF _{ee} 1/3.0 0.333 0.333)x)x)x)x	F _{LOC} 1 1	x F _{elechea} x 1 x 1 x 1 x 1	at))))	0.49 0.49	/ 9/6/3	5/3.412 3.412 801							
ΔkW ΔkW ΔkW	-	units 1 0.071	x(x	ΔkW 0.071	/	unit)																						
ΔMMBtu ΔMMBtu ΔMMBtu Δfuel oil	= = = = EEM-4d	units 1 13.410 96	x(x(x(GPD 21.463	x x	365 365 549	x x 94760.566	8.33 8.33	x x	ΔT _{main} 140 -55.8	y y y	1000000 1000000 1000000	×((FFFDHW 1.0 1.0	/ /	UEFbaseline 0.8400 0.8400)+(FboilerDH)+(1/)+(IW / AF 80 1.25			ee 0.333	x x x	Floc 1 1	x x x	Ffuelheat 0 0	x x x	Fheat/AFUE 0.49/80% 0.6125)))
Τοταί Δκψη Τοταί ΔkW Δfuel oil Δ\$ kWh Δ\$ fuel oil	=	5603 0.071 119.731 \$933.13 \$177.69																										

EEM-5: Kitchen Appliances																
Refrigerator_		Refrigerator														
CF, coincidence factor	1	ΔkWh	=	units	x(kWh _{baseline}	-	kWh _{ee})x(1	+	HVAC _c)			
$HVAC_{c}$, interaction factor for annual elec energy consumption	0.066	ΔkWh	=	4	x(495	-	214)x(1	+	0.066)			
$HVAC_{d}$, interaction factor at utility summer peak hour	0.175	ΔkWh	=	4	x(281)x(1.066)			
HVAC _{ff} , interaction factor for annual fossil fuel consumption	-0.002	ΔkWh	=	1198.184												
8,760, hours in one year																
kWh _{baseline} , US federal standard	495	ΔkW	=	units	x(kWh _{baseline}	-	kWh _{ee}	/	8760)x(1	+	HVAC _d)x	CF
kWh _{ee} , ENERGY STAR	214	ΔkW	=	4	x(495	-	214	/	8760)x(1	+	0.175)x	1
		ΔkW	=	4	x(281		/	8760)x(1.175)x	1
page - 381		ΔkW	=	0.151												
		ΔMMBtu	=	units	x(kWh _{baseline}	-	kWh _{ee})x	HVAC _{ff}						
		ΔMMBtu	=	4	x(495	-	214)x	-0.002						
		ΔMMBtu	=	4	x(281)x	-0.002						
		ΔMMBtu	=	-2.248												
		ΔFuel Oil	=	-16												
lce maker		Ice Maker														
kWh _{baseline} , Batch type, self-contained	10.3345	ΔkWh	=	units	x(kWh _{baseline}	-	kWh _{ee})x	365	х	Cycle	x(IHR/100)	
kWh _{ee} , Batch type, self-contained	8.7795	ΔkWh	=	1	x(10.3345	-	8.7795)x	365	х	0.75	x(95/100)	
Cycle, compressor duty cycle	0.75	ΔkWh	=	1	х(1.5550)x	365	х	0.75	x(0.95)	
IHR - Ice Harvest Rate	95	ΔkWh	=	404.397												
CF, coincidence factor	0.9															
255		ΔkW	=	((ΔkWh	/(8,760	х	Cycle))x	CF						
page - 355		ΔkW ΔkW	=	((51363.982 0.055	/(8,761	х	0.75))x	0.9						
		ZKVV	=	0.055												
Kitchen Demand Control Ventilation		Kitchen Demand Co	ontrol Ver	tilation												
page 583 - kitchen demand control vent		<u>ΔkWh</u>	=	units	х	hp	x(∆kWh/hp)							
		ΔkWh	=	1	x	1	×(4423)							
hp- horsepower of exhaust fan	1	ΔkWh	=	4423												
ΔkWh/hp	4,423															
258 cfm / linear foot	3,870	ΔkW	=	units	х	hp	×(ΔkW/hp)x	CF						
kilowatts kilowatts to hp	1.161 0.865758	ΔkW ΔkW	=	1 0.81	٦ ×	1	x(0.9)x	0.9						
ΔkW/hp	0.602758	Δκνν	=	0.61												
CF, coincidence factor	0.9	ΔMMBtu	=	units	x	hp	х	ΔMMBtu/hp								
ΔMMBtu/hp (Poughkeepsie)	25	ΔMMBtu	=	1	x	1	x	25								
		ΔMMBtu	=	25												
		ΔFuel Oil	=	179												
		Total ∆kWh	=	6026	٦											
		Total ΔkW	=	1.016												

Total ∆kWh	=	6026
Total ∆kW	=	1.016
Δ\$ kWh	=	\$1,003.51
Total ∆ Fuel Oil	=	163
Total ∆\$ Fuel Oil	=	\$241.18

BUDGET PRICING



Mechanical/Electrical Engineering Consultants 60 LAKEFRONT BLVD, SUITE 320 BUFFALO, NY 14202

Budget Pricing Cost Estimate

PROJECT NAME	E: Rhinebeck V	'illage Hall	
M/E REFERENC	E: 211222	DATE:	2/14/2022
DIVISION:	ENERGY	BY:	KEW

ITEM	DESCRIPTION	QTY.	UNIT	LABOR COST	MATERIAL COST	TOTAL ITEM COST
EEM-1: High-Efficier	ncy Lighting					
	Code Compliant Fixtures - Office	8200	SF	\$1.50	\$0.80	\$18,860
	Code Compliant Fixtures - Firetruck	3600	SF	\$1.50	\$0.80	
	TOTAL BASECASE					\$27,140
	LED Lighting & Controls-Office	8200	SF	\$1.50	\$1.00	\$20,500
	LED Lighting & Controls-Firetruck	3600	SF	\$1.50	\$1.00	\$9,000
	TOTAL PROPOSED					\$29,500
	EEM-1 TOTAL INCREMENTAL COST					\$29,500
EEM-2: Envelope Im	nprovements					
	Existing Roof To Remain	5400	SF	\$0.00	\$0	\$0
	Existing Walls To Remain	6888	SF	\$0.00	\$0	\$0
	TOTAL BASECASE					\$0
EEM-2	Add Roof, 4" insulation R-30 total	5400	SF	\$12.00	\$4.94	\$91,449
	Furr out Walls, 3.5" studs with 4" batt insul	6888	SF	\$3.75	\$2.66	. ,
	Ceiling System - Air Barrier	5400	SF	\$0.75	\$0.50	. ,
	TOTAL EEM-2 PROPOSED	0.000	01	\$94,644.96	\$47,659.57	\$142,305
	EEM-2 TOTAL INCREMENTAL COST					\$142,305
EEM-3: HVAC Option	<u>ns *</u>					
EEM-3a Code RTU	with DX cooling					
	Code RTU with DX cooling	1	EA	\$51,209.50	\$67,737	\$118,947
EEM-3b High Efficie	nt RTU with DX cooling					
	High Eefficient RTU with DX cooling, energy recovery	1	EA	\$58,890.93	\$101,267	\$160,158
EEM-3c High Efficier	nt Heat Pump				, - , -	+ ,
	RTU w/ enthalpy ER, high efficiency	1	EA	\$61,507.75	\$151,395	\$212,902
EEM-3d VRF System	n					
	DOAS w/ enthalpy ER, high efficiency	1	EA	\$6,158.25	\$9,665	\$15,823
	VRF System	1	EA	\$96,496.50	\$128,186.59	\$224,683
	Total VRF			\$102,654.75	\$137,851.59	\$240,506

ITEM	DESCRIPTION	QTY.	UNIT	LABOR COST	MATERIAL COST	TOTAL ITEM COST
EEM-3e Geothermal	System					
	Geothermal wells (23 tons)	10	EA	\$17,250.00	\$5,750	\$230,000
	Heat Pumps	2	EA	\$5,175.00	\$6,497.50	\$23,345
	Piping	1	LS	\$8,625.00	\$8,625.00	\$17,250
	Controls	1	LS	\$17,250.00	\$17,250.00	\$34,500
	HP AHUs	2	EA	\$13,397.50	\$41,745.00	\$110,285
	Pumps	2	EA	\$8,414.17	\$27,485.00	\$71,798
	Total Geothermal			\$199,678.33	\$125,465.00	\$487,178
	EEM-3a TOTAL INCREMENTAL COST					\$118,947
	EEM-3b TOTAL INCREMENTAL COST					\$160,158
	EEM-3c TOTAL INCREMENTAL COST					\$212,902
	EEM-3d TOTAL INCREMENTAL COST					\$240,506
	EEM-3e TOTAL INCREMENTAL COST					\$487,178
EEM-4: DHW Options	<u>s</u>					
EEM-4a DHW Propa	ne Fired Unit					
	50 gallon propane fired	3	EA	\$1,080.00	\$2,500	\$10,740
EEM-4b DHW Electri	ic Unit					
	50 gallon unit	3	EA	\$1,080.00	\$2,000	\$9,240
EEM-4c DHW Air Sol	urce Heat Pump					
	50 gallon , heat pump type	3	EA	\$1,080.00	\$4,328	\$16,224
EEM-4d DHW Geothe	ermal Well Field					
	50 gallon water to water heat pump system	3	EA	\$1,080.00	\$5,328	\$19,224
	EEM-4a TOTAL INCREMENTAL COST					\$10,740
	EEM-4b TOTAL INCREMENTAL COST					\$9,240
	EEM-4c TOTAL INCREMENTAL COST					\$16,224
	EEM-4d TOTAL INCREMENTAL COST					\$19,224
EEM-5: Kitchen Appl	iance Replacement					
	Exisiting Refrigerator remain	4	EA	\$0.00	\$0	\$0
	Exisiting Ice Maker	1	EA	\$0.00	\$0	\$C
	NO heat/smoke control	1	EA	\$0.00	\$0	\$C
	ENERGY Star Refrigerator	4	EA	\$450.00	\$2,750	\$12,800
	ENERGY Star Ice Maker	1	EA	\$450.00	\$678	\$1,128
	Demand Control Ventilation	1	EA	\$450.00	\$1,049	\$1,499
	TOTAL EEM-5 INCREMENTAL COST					\$15,427

Pricing from RSMeans Building Cost Data. Includes differences between options and items related to energy efficiency.

* Energy Efficeincy Measure pricing does not include costs associated with contingincies, TAB, design fees, electrical upgrades, general construction related costs etc. (unless otherwise identified).

MAINTENACE COST



Mechanical/Electrical Engineering Consultants 60 LAKEFRONT BLVD, SUITE 320 BUFFALO, NY 14202

Annual Maintenance	Cost Estimate
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PROJECT NAME: H	Rhinebeck Vill	age Hall	
M/E REFERENCE:	211222	DATE:	2/14/2022
DIVISION:	ENERGY	BY:	KEW

ITEM	DESCRIPTION	QTY.	UNIT	LABOR COST	MATERIAL COST	TOTAL ITEM COST
EEM-1: High-Efficiency	/Lighting_					
	LED Lighting & Controls-Office	8200	SF	\$0.50	\$0.25	\$6,150
	LED Lighting & Controls-Firetruck	3600	SF	\$0.50	\$0.25	\$2,700
	TOTAL PROPOSED					\$8,850
	EEM-1 TOTAL INCREMENTAL COST					\$8,850
EEM-2: Envelope Imp	rovements					
	Add Roof, 6" insulation R-30	5400	SF	\$0.00	\$0	\$0
	Furr out Walls, 3.5" studs with 4" batt insul	6888	SF	\$0.00	\$0	\$0
	Ceiling System	5400	SF	\$0.00	\$0	
	TOTAL EEM-2 PROPOSED			\$0.00	\$0.00	\$0
	EEM-2 TOTAL INCREMENTAL COST					\$0
EEM-3: HVAC Options	*					
EEM-3a Code RTU wit	th DX cooling					
	Code RTU with DX cooling	1	EA	\$550.00	\$325	\$875
EEM-3b High Efficient	RUT with DX cooling					
	High Eefficient RTU with DX cooling, energy recovery	1	EA	\$550.00	\$423	\$973
EEM-3c High Efficient	Heat Pump					
_	RTU w/ enthalpy ER, high efficiency	1	EA	\$550.00	\$549	\$1,099
EEM-3d VRF System						
	DOAS w/ enthalpy ER, high efficiency	1	EA	\$550.00	\$150	\$700
	VRF System	1	EA	\$500.00	\$250.00	\$750
	Total VRF			\$1,050.00	\$400.00	\$1,450

ITEM	DESCRIPTION	QTY.	UNIT	LABOR COST	MATERIAL COST	TOTAL ITEM COST
EEM-3e Geothermal	System					
	Geothermal wells (19 tons)	20	EA	\$0.00	\$0	\$0
	Heat Pumps	10	EA	\$450.00	\$423.00	\$8,730
	Pumps	2	EA	\$258.00	\$320.00	\$1,156
	Total Geothermal			\$5,016.00	\$4,870.00	\$9,886
	EEM-3a TOTAL INCREMENTAL COST					\$875
	EEM-3b TOTAL INCREMENTAL COST					\$973
	EEM-3c TOTAL INCREMENTAL COST					\$1,099
	EEM-3d TOTAL INCREMENTAL COST					\$1,450
	EEM-3e TOTAL INCREMENTAL COST					\$9,886
EEM-4: DHW Options	<u>1</u>					
EEM-4a DHW Gas Fil	red Unit					
	3, 50 gallon gas fired	3	EA	\$100.00	\$125	\$675
EEM-4b DHW Air Sou	urce Heat Pump					
	3, 50 gallon , heat pump type	3	EA	\$100.00	\$145	\$735
EEM-4c DHW Geothe	ermal Well Field					
	3, 50 gallon water to water heat pump	3	EA	\$100.00	\$178	\$834
	EEM-4a TOTAL INCREMENTAL COST					\$675
	EEM-4b TOTAL INCREMENTAL COST					\$735
	EEM-4c TOTAL INCREMENTAL COST					\$834
EEM-5: Kitchen Appli	ance Replacement					
	ENERGY Star Refrigerator	4	EA	\$100.00	\$100	\$800
	ENERGY Star Ice Maker	1	EA	\$100.00	\$100	\$200
	Demand Control Ventilation	1	EA	\$100.00	\$100	\$200
	TOTAL EEM-5 INCREMENTAL COST					\$1,200

Pricing from RSMeans Facility Maintenance & Repair Data. Includes differences between options and items related to energy efficiency.

* Maintenance pricing does not include costs associated with other trades(unless otherwise identified).

PHOTOS





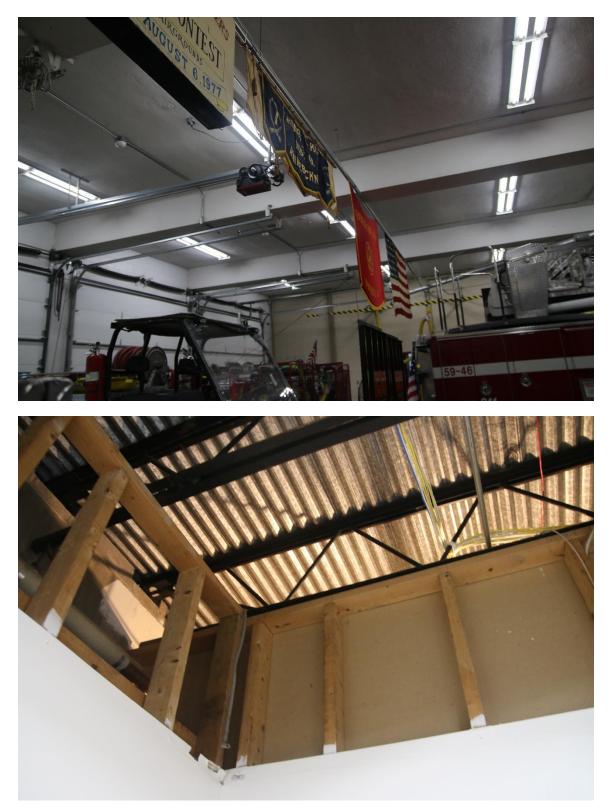




M/E Reference 211222





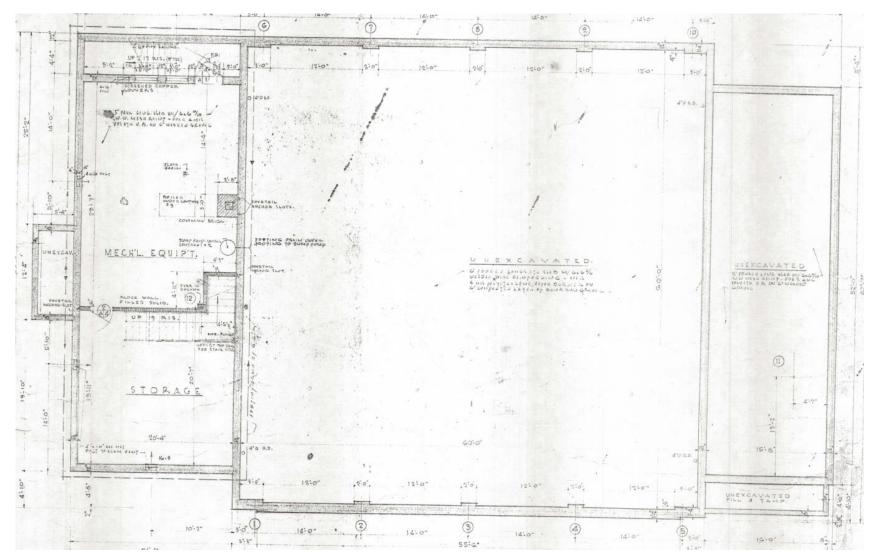






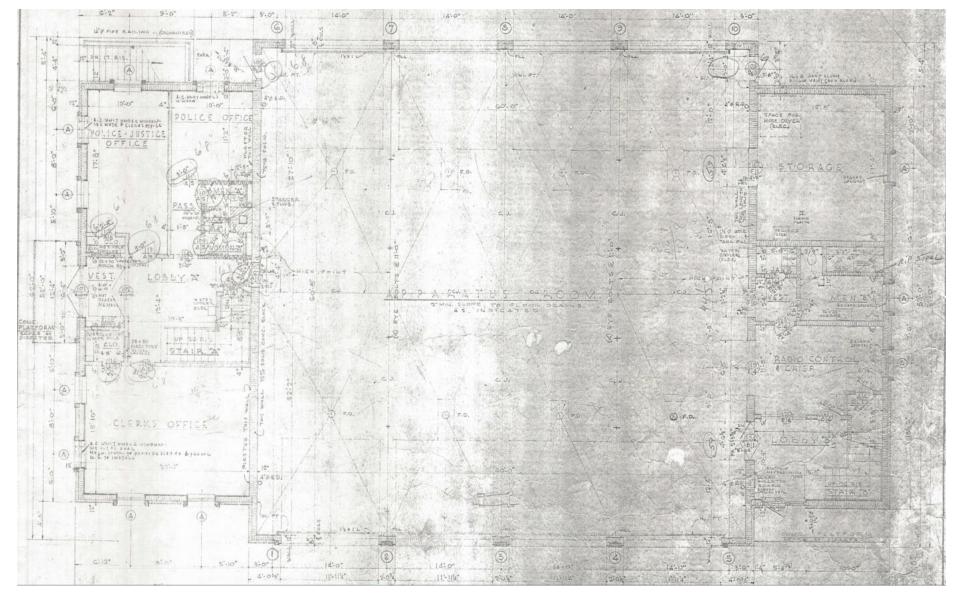
FLOOR PLANS

Basement Floor Plan



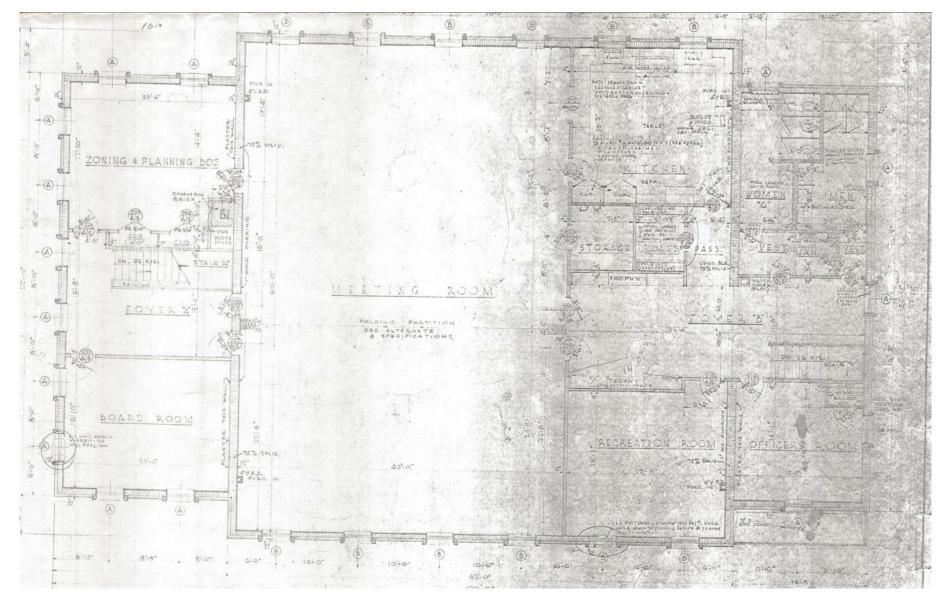
M/E Reference 211222

First Floor Plan



M/E Reference 211222

Second Floor Plan



INCENTIVE PROGRAMS

Many of the measures are eligible for implementation incentives through the Central Hudson Gas & Electric incentive programs. An estimate of the impact these incentives could have on the various measures are shown below. Please note that the incentive programs are updated and change regularly, and are subject to program requirements and eligibility, and therefore are not guaranteed

EEM No.	Energy Efficiency Measure Description	Annual Electric Savings [kWh]	Demand	Cost Savings	Annual #2 Fuel Oil Savings [gallons]	0	Annual #2 Fuel Oil Cost Savings [\$]	Total Energy Consumption Savings [mmBtu]	Total Annual Cost Savings [\$]	Estimated EEM Cost [\$] (total)	Simple Payback [Years]	Incentive*	Estimated EEM Cost [\$] (incremental, w/ incentives)	Simple Payback w/ Incentives [Years]
1	High-Efficiency Lighting	15,500	7.71	\$2,581.46	-185	-25.96	-\$275.16	26.95	\$2,306.30	\$29,500.00	12.8	\$2,600.00	\$26,900.00	11.7

*Central Hudson Gas & Electric has programs for one for one lighting replacement, individual controls, and performanced based incentives, subject to program requirements, verify incentive elligibility with utility. Incentives are not guaranteed.

Incentives are available for LED fixtures that are listed are ENERGY Star or DLC listed. The incentives range from \$15-\$25 per interior fixture, \$50-75 for high bay fixtures, \$45-75 for exterior fixtures, and \$10-\$20 for controls, from a prequalified list on the Central Hudson Gas and Electric website.

EEM No.	Energy Efficiency Measure Description	Annual Electric Savings [kWh]	Electric Peak Demand Savings [kW]	Annual Electric Cost Savings [\$]	Annual #2 Fuel Oil Savings [gallons]	Annual #2 Fuel Oil Savings [mmBtu]	Annual #2 Fuel Oil Cost Savings [\$]	Total Energy Consumption Savings [mmBtu]	Total Annual Cost Savings [\$]	Estimated EEM Cost [\$] (total)	Simple Payback [Years]	Incentive	Estimated EEM Cost [\$] (incremental, w/ incentives)	Incentives
2	Envelope Improvements - Roof and Walls	2,351	2.19	\$391.59	1,114	155.92	\$1,652.88	163.95	\$2,044.47	\$142,304.53	69.6	*	\$142,304.53	69.6

*Central Hudson Gas & Bectric has programs for performance based incentives, subject to program requirements, verify incentive elligibility with utility. Incentives are not guaranteed.

EEM No.	Energy Efficiency Measure Description	Annual Electric Savings [kWh]	Electric Peak Demand Savings [kW]	Annual Electric Cost Savings [\$]	Annual #2 Fuel Oil Savings [gallons]	Oil	Annual #2 Fuel Oil Cost Savings [\$]	Total Energy Consumption Savings [mmBtu]	Total Annual Cost Savings [\$]	Estimated EEM Cost [\$] (total)	Simple Payback [Years]	Incentive*	Estimated EEM Cost [\$] (incremental, w/ incentives)	Incentives
3a	Code RTU with DX cooling	-113,144	4.46	-\$18,843.10	4,329	606.00	\$6,423.90	219.84	-\$12,419.20	\$118,946.80	-9.6	\$920.00	\$118,026.80	-9.5
*Centra	l Hudson Gas & Electric has pr	ograms for I	-IVAC incer	ntives, \$40/ton fo	or packaged	l units, subje	ect to program	requirements, ver	ify incentive elli	gibility with utility	. Incentives	are not guarante	eed.	

EEM No.		Annual Electric Savings [kWh]	Demand	Savings	Oil	Annual #2 Fuel Oil Savings [mmBtu]	Annual #2 Fuel Oil Cost Savings [\$]	Total Energy Consumption Savings [mmBtu]	Total Annual Cost Savings [\$]	Estimated EEM Cost [\$] (total)	Simple Payback [Years]	Incentive*	Estimated EEM Cost [\$] (incremental, w/ incentives)	Incentives
3b	High Efficient RTU with DX cooling	-93,463	8.82	-\$15,565.50	5,045	706.25	\$7,486.60	387.26	-\$8,078.90	\$160,158.19	-19.8	\$920.00	\$159,238.19	-19.7

*Central Hudson Gas & Bectric has programs for HVAC incentives, \$40/ton for packaged units, subject to program requirements, verify incentive elligibility with utility. Incentives are not guaranteed.

EEM No.	Energy Efficiency Measure Description	Annual Electric Savings [kWh]	Demand	Savings	Annual #2 Fuel Oil Savings [gallons]	Annual #2 Fuel Oil Savings [mmBtu]	Savings	Total Energy Consumption Savings [mmBtu]	Total Annual Cost Savings [\$]	Estimated EEM Cost [\$] (total)	Simple Payback [Years]	Incentive*	Estimated EEM Cost [\$] (incremental, w/ incentives)	Incontivos
3c	High Efficient Heat Pump	3,226	10.12	\$537.28	5,045	706.25	\$7,486.60	717.26	\$8,023.88	\$212,902.31	26.5	\$46,977.75	\$165,924.55	20.68

* Incentives are not guaranteed, Central Hudson Gas & Electric has programs for clean heat program, assuming \$200/mmbtu saved, capped at 50% incremental cost, performance based incentives, subject to program requirements, verify incentive elligibility with utility.

EEM No.	Energy Efficiency Measure Description	Annual Electric Savings [kWh]	Electric Peak Demand Savings [kW]	Cost Savings	Annual #2 Fuel Oil Savings [gallons]	0	Annual #2 Fuel Oil Cost Savings [\$]	Total Energy Consumption Savings [mmBtu]	Total Annual Cost Savings [\$]	Estimated EEM Cost [\$] (total)	Simple Payback [Years]	Incentive*	Estimated EEM Cost [\$] (incremental, w/ incentives)	Incontivos
3d	VRF System	5,067	12.53	\$843.84	5,045	706.25	\$7,486.60	723.54	\$8,330.44	\$240,506.34	28.9	\$60,779.77	\$179,726.57	21.6
* Incent	tives are not guaranteed, Centr	al Hudson G	Sas & Electri	c has programs	for clean h	eat program	, assuming \$20	00/mmbtu saved, o	apped at 50%	incremental cost	, performan	ce based incenti	ves, subject to prog	gram

requirements, verify incentive elligibility with utility.

NYS Clean Heat Statewide Heat Pump Incentive Program could be leveraged for implementation incentives.

	EM lo.	Energy Efficiency Measure Description	Annual Electric Savings [kWh]	Demand	Annual Electric Cost Savings [\$]	Annual #2 Fuel Oil Savings [gallons]	Annual #2 Fuel Oil Savings [mmBtu]	Annual #2 Fuel Oil Cost Savings [\$]	Total Energy Consumption Savings [mmBtu]	Total Annual Cost Savings [\$]	Estimated EEM Cost [\$] (total)	Simple Payback [Years]	Incentive*	Estimated EEM Cost [\$] (incremental, w/ incentives)	Incentives
:	Be	Geothermal System	6,144	10.09	\$1,023.20	5,045	706.25	\$7,486.60	727.22	\$8,509.80	\$487,178.33	57.2	\$145,443.77	\$341,734.57	40.2

* Incentives are not guaranteed, ConEdison has programs for clean heat program, assuming \$200/mmbtu saved, capped at 50% incremental cost, performance based incentives, subject to program requirements, verify incentive elligibility with utility.

There are significant implementation incentives that are available which could help mitigate the higher first cost of GSHP systems.

EEM No.	Energy Efficiency Measure Description	Annual Electric Savings [kWh]	Electric Peak Demand Savings [kW]	Savings	Annual Fossil Fuel Savings [gallons]	Annual Fossil Fuel Savings [mmBtu]	181	Total Energy Consumption Savings [mmBtu]	Total Annual Cost Savings [\$]	Estimated EEM Cost [\$] (total)	Simple Payback [Years]	Incentive	Estimated EEM Cost [\$] (incremental, w/ incentives)	Incontivos
4a	DHW Propane Fired Unit	7,676	0.17	\$1,278.44	-48	0.70	-\$233.95	26.90	\$1,044.48	\$10,740.00	10.3	\$0.00	\$10,740.00	10.3

EEM No.	Energy Efficiency Measure Description	Annual Electric Savings [kWh]	Demand	Annual Electric Cost Savings [\$]	Annual #2 Fuel Oil Savings [gallons]	0	Savings	Total Energy Consumption Savings [mmBtu]	Total Annual Cost Savings [\$]	Estimated EEM Cost [\$] (total)	Simple Payback [Years]	Incentive	Estimated EEM Cost [\$] (incremental, w/ incentives)	Simple Payback w/ Incentives [Years]
4b	DHW Electric Unit	224	0.04	\$37.27	120	16.76	\$177.69	17.53	\$214.96	\$9,240.00	43.0	\$0.00	\$9,240.00	43.0

EEM No.	Energy Efficiency Measure Description	Annual Electric Savings [kWh]	Electric Peak Demand Savings [kW]	Annual Electric Cost Savings [\$]	Annual #2 Fuel Oil Savings [gallons]	Annual #2 Fuel Oil Savings [mmBtu]	Annual #2 Fuel Oil Cost Savings [\$]	Total Energy Consumption Savings [mmBtu]	Total Annual Cost Savings [\$]	Estimated EEM Cost [\$] (total)	Simple Payback [Years]	Incentive*	Estimated EEM Cost [\$] (incremental, w/ incentives)	Incontivos
4c	DHW Air Source Heat Pump	5,019	0.06	\$835.90	120	16.76	\$177.69	33.89	\$1,013.59	\$16,224.00	16.0	\$2,000.00	\$14,224.00	14.0

* Incentives are not guaranteed, Central Hudson Gas and Electric has programs for clean heat program, assumes \$1000/w ater heater <120 gallon tank capacity, subject to program requirements, verify incentive elligibility with utility.

EEM No.	Energy Efficiency Measure Description	Annual Electric Savings [kWh]	Electric Peak Demand Savings [kW]	0	Annual #2 Fuel Oil Savings [gallons]	0	Annual #2 Fuel Oil Cost Savings [\$]	Total Energy Consumption Savings [mmBtu]	Total Annual Cost Savings [\$]	Estimated EEM Cost [\$] (total)	Simple Payback [Years]	Incentive*	Estimated EEM Cost [\$] (incremental, w/ incentives)	Simple Payback w/ Incentives [Years]
4d	DHW Geothermal Well Field	5,603	0.07	\$933.13	120	16.76	\$177.69	35.89	\$1,110.82	\$19,224.00	17.3	\$2,000.00	\$17,224.00	15.5

* Incentives are not guaranteed, Central Hudson Gas and Electric has programs for clean heat program, assumes \$1000/w ater heater <120 gallon tank capacity, subject to program requirements, verify incentive elligibility with utility.

EEM No.		Annual Electric	Electric Peak Demand Savings [kW]	0	Annual #2 Fuel Oil Savings [gallons]	Oil	Savings	Total Energy Consumption Savings [mmBtu]	Total Annual Cost Savings [\$]	Estimated EEM Cost [\$] (total)	Simple Payback [Years]	Incentive*	Estimated EEM Cost [\$] (incremental, w/ incentives)	Simple Payback w/ Incentives [Years]
5	Appliance Replacement	6,026	1.02	\$1,003.51	163	22.75	\$241.18	43.32	\$1,244.69	\$15,427.00	12.4	*	\$15,427.00	12.4

* Central Hudon Gas and Electric has programs for performance based incentives, subject to program requirements, verify incentive elligibility with utility. Incentives are not guaranteed.

See below for a description of several potential incentive programs.

NYSERDA NEW CONSTRUCTION PROGRAM

***Applicable to <u>All-Electric</u> Projects Only

Support Level 1 – First Look:

- For Carbon Neutral Ready projects of any square footage and at any design phase prior construction.
 - Projects greater than 15,000 square feet and in schematic design phase or earlier may transition to Support Level 2 upon completion of the First Look, provided the Applicant commits to a Carbon Neutral Ready or better design.
- Technical Support provided by a NYSERDA-approved Primary Energy Consultant:
- Meet with the Applicant to review design phase plans or proposed equipment selections, and
- Provide a summary of energy savings suggestions.
- NYSERDA contribution for Support Level 1:
 - Technical Support is provided at no cost to the Applicant.
 - Fixed fee schedule for Primary Energy Consultant:
 - Projects up to 10,000 SF \$1,500
 - Projects 10,001 to 30,000 SF \$3,000
 - Projects over 30,000 SF \$5,000
- Support Level 2 Carbon Neutral Ready (>15,000 SF)
 - Project must be all electric, including cooking, laundry, domestic hot water, etc. The only exception is an emergency generator.
 - Energy Modeling, Analysis and Report:
 - Engage with the Applicant and project design team to identify, model and analyze potential energy savings and electrification opportunities. Include analysis of ventilation and related building envelope and HVAC system needs to optimize buildings to meet COVID-19 related health and safety guidance.
 - Integrated Project Delivery:
 - Provide additional technical support for Applicants who incorporate and execute Integrated Project Delivery in the project design.
 - Smart Buildings:
 - Provide additional technical support for Applicants who incorporate and execute a suite of Smart Building features in the project design and construction.
 - Embodied Carbon:
 - Suggest, evaluate and quantify embodied carbon reduction opportunities. Prepare and submit a separate report of the embodied carbon analysis to the Applicant and NYSERDA.
 - NYSERDA Contribution:
 - NYSERDA will pay 100% of the technical support costs, including energy modeling and efficiency measure analysis, up to a maximum \$200,000.
 - For projects seeking to reduce embodied carbon by at least 20%, NYSERDA will pay an additional 10% of the Technical Support costs to identify and quantify strategies that reduce embodied carbon.
 - Incentive of **\$2/sf** if source energy is a least 15% less than a code-compliant baseline
 - For more information: <u>Commercial New Construction Program NYSERDA</u>

NYS CLEAN HEAT PROGRAM

NYS Clean Heat Statewide Heat Pump Program

- Heat pump system options only. Must utilize heat pump for heating.
- Custom performance incentives per MMBtu saved, according to type and size of full load heating capacity OR per equipment if smaller sizes
- Must utilize NYSERDA-participating contractor or designer, subject to installation requirements

For more information: <u>clean-heat-program-guide.pdf</u> and <u>https://ch-nyshp.programprocessing.com/</u>

ELECTRIC VEHICLE CHARGING STATIONS

NYSERDA Charge Ready NY

- \$4,000 per charging port for Level 2 charging stations
- For additional information: <u>NYSERDA Charge Ready NY</u>

Central Hudson Gas and Electric Vehicle PowerReady - Infrastructure

- Two categories of equipment or infrastructure are eligible for incentives under the EV Make-Ready Program:
 - Utility-side Make-Ready Infrastructure: Utility electric infrastructure needed to connect and serve a new EV charger. This may include traditional distribution infrastructure such as step-down transformers, overhead service lines, and utility meters that will continue to be owned and operated by the utility.
 - Customer-side Make-Ready Infrastructure: EV equipment or infrastructure necessary to make a site ready to accept an EV charger that is owned by the charging station Developer, Equipment Owner, or Site Host. This electric infrastructure may include conductors, trenching, and panels needed for the EV charging station.
- EV Charging in Disadvantaged Communities may be eligible for higher incentive level.
- For additional information: <u>https://www.cenhud.com/en/my-energy/electric-vehicles/business-</u> charging-incentives/NYS Electric Vehicle Recharging Property Tax Credit
- Credit the lesser of \$5,000 or 50% of the cost of property less any cost paid from the proceeds of grants
- For additional information: NYS Electric Vehicle Recharging Property Tax Credit

CENTRAL HUDSON GAS AND ELECTRIC

- Commercial customers needing energy efficient improvements and flexibility to match project characteristics for lighting, HVAC (including ground and air-source heat pumps, refrigeration and plug loads.
- Commercial kitchen equipment.
- For additional information : https://www.cenhud.com/en/my-energy/save-energy-money/

FEDERAL ENERGY-EFFICIENCY TAX DEDUCTION

<u>179D Commercial Buildings Energy-Efficiency Tax Deduction</u>

- \$1.80/sf deduction (adjusted annually) for property exceeding 50% energy savings utilizing the latest version of ASHRAE 90.1
- Partial deductions available for individual reductions for only envelope, HVAC/DHW, and lighting

For additional information: <u>179D Commercial Buildings Energy-Efficiency Tax Deduction</u>